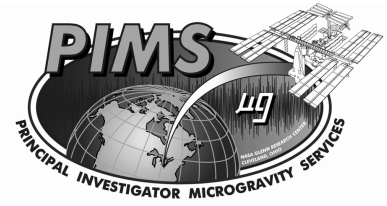


Section 18
ISS Design Analysis Cycle & Environment Predictions

Microgravity Environment Interpretation Tutorial
NASA Glenn Research Center
March 5-7, 2002

Steve Del Basso

Structural Analysis Microgravity Team
Boeing
502 Gemini Avenue
Houston, Texas
281-226-4069

Presentation Overview

- Design Analysis Cycle
- Analysis Methods
- Active Rack Isolation System
- Disturbance Forcing Functions
- Quasi-steady Accelerations
- Vibratory Accelerations
- Correlation & Update
- Summary

Design Analysis Cycles

DACs may be viewed as PDR/CDR level analyses or "special" case studies.

- DAC8 was completed in winter 1999.
- DAC9 is in process and will be completed in the summer of 2002.
- DACs capture updated models & disturbance forcing functions.

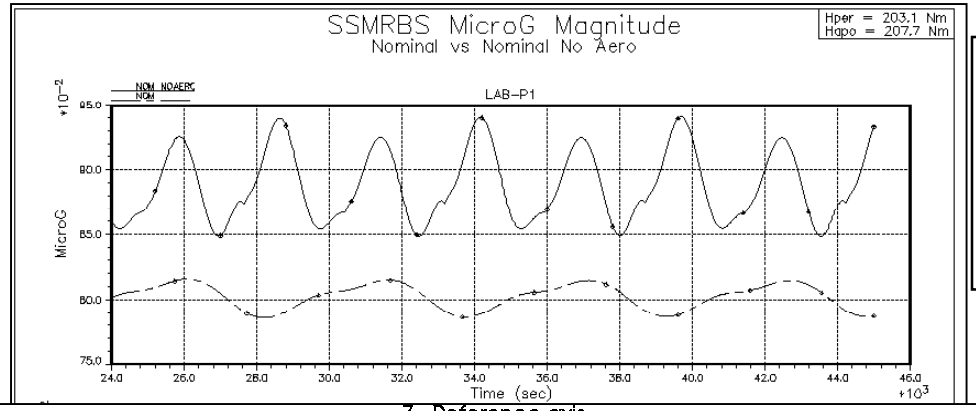
Verification Analysis Cycles (VACs) are in process and are conducted on a flight by flight basis.

- Verify that the hardware launched complies with Assembly Complete microgravity requirements.
- Priority tasks necessary for Certification of Flight Readiness.

Microgravity sustaining engineering efforts underway

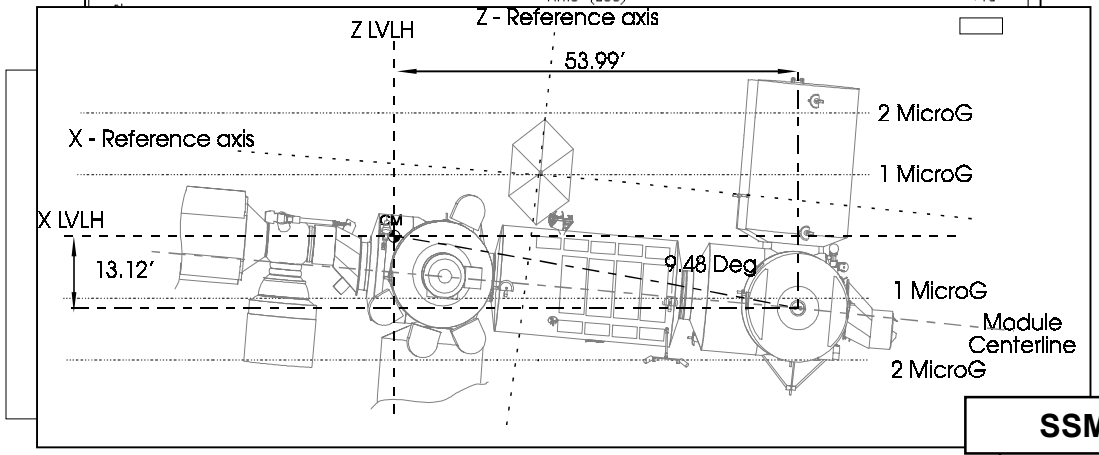
- Use of on-orbit measurements for issue resolution, uncertainty reduction, analytical model correlation.
- Support anomaly resolution and operations.

Methods & Tools
Quasi-Steady Analysis



Below 0.01 Hz

- **Orbital Mechanic Multi-Rigid Body Closed Loop Attitude Control Analysis**
- **Space Station Multi Rigid Body Simulation (NASA SPARC)**
- **SSMRBS used for GN&C Software Verification**



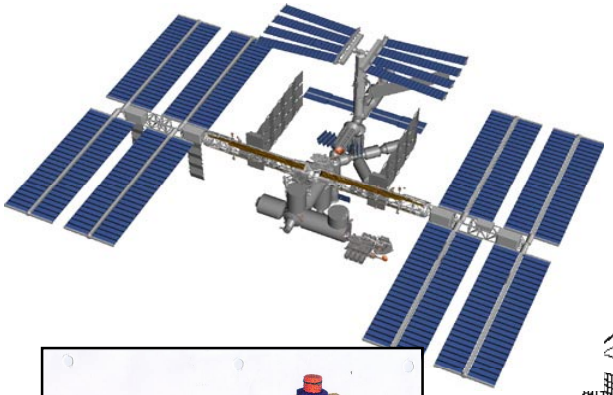
$$\vec{a} = -\mu\left(\frac{\vec{r}_p}{r_p^3} - \frac{\vec{r}_g}{r_g^3}\right) - \vec{\omega}\times\left(\vec{\omega}\times\vec{r}_{p/g}\right) - \dot{\vec{\omega}}\times\vec{r}_{p/g} + \vec{a}_D$$

Gravity Gradient | Centripetal | Tangential | Aerodynamic Drag

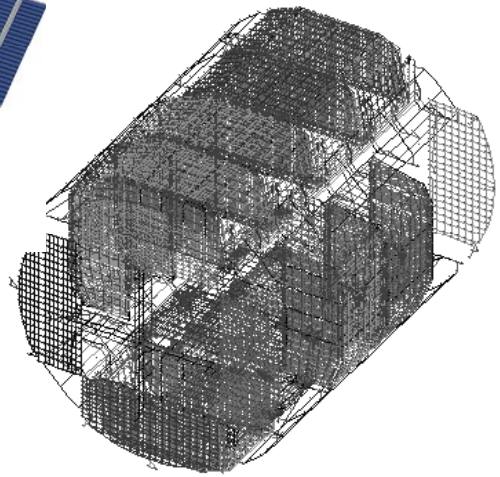
SSMRBS Environment Data Validation

verify_gfield (gravity)	verify_bfield (magnetic)	verify_atm_density (density)
ADA Advanced Simulation Development System (ASDS) Gravitational Potential (GOTPOT) model	Goddard Space Flight Center International Geophysical Reference Field (IGRF) Earth Magnetic model	Marshall Engineering Thermosphere (MET) Earth Atmospheric Density model

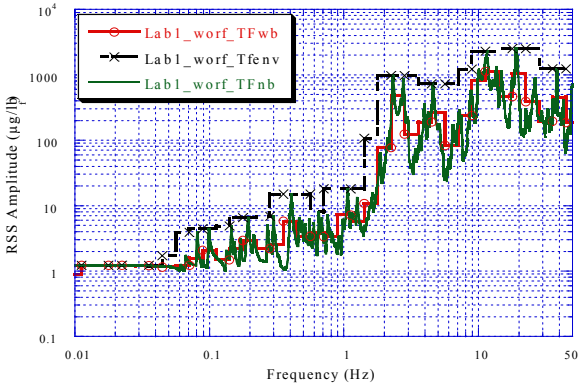
Methods & Tools
Structural Dynamic Analysis

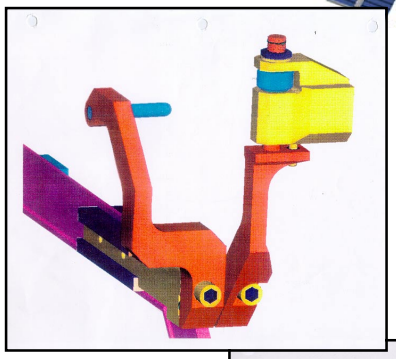


Enhanced COF Model

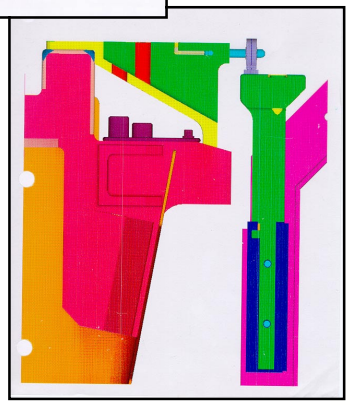


0.01 to 50 Hz
Structural Dynamic Finite Element Analysis
MSC/NASTRAN (NASA CRAY)
"Enhanced" Loads & Dynamics Models





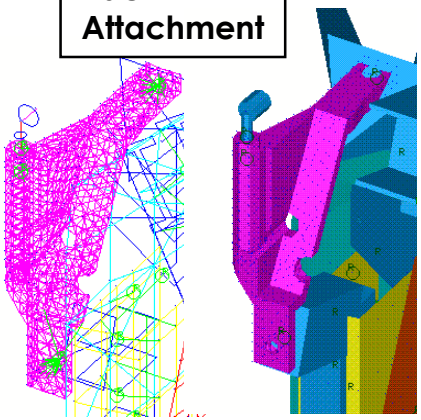
Lower Pivot

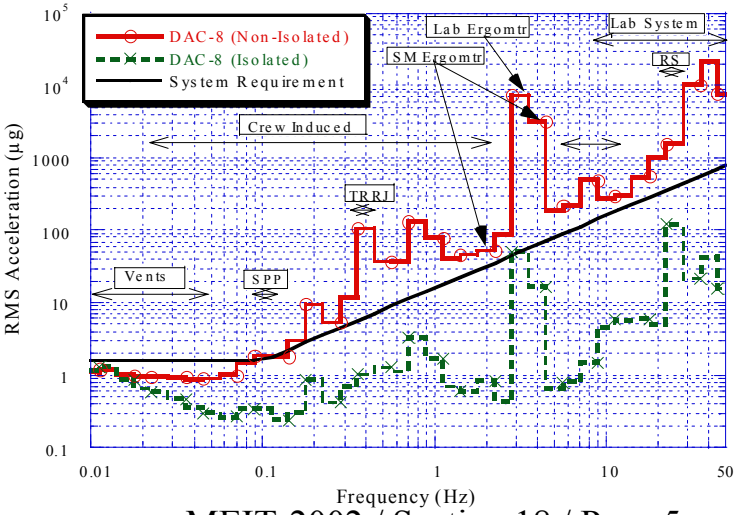


Non-isolated Rack I/F

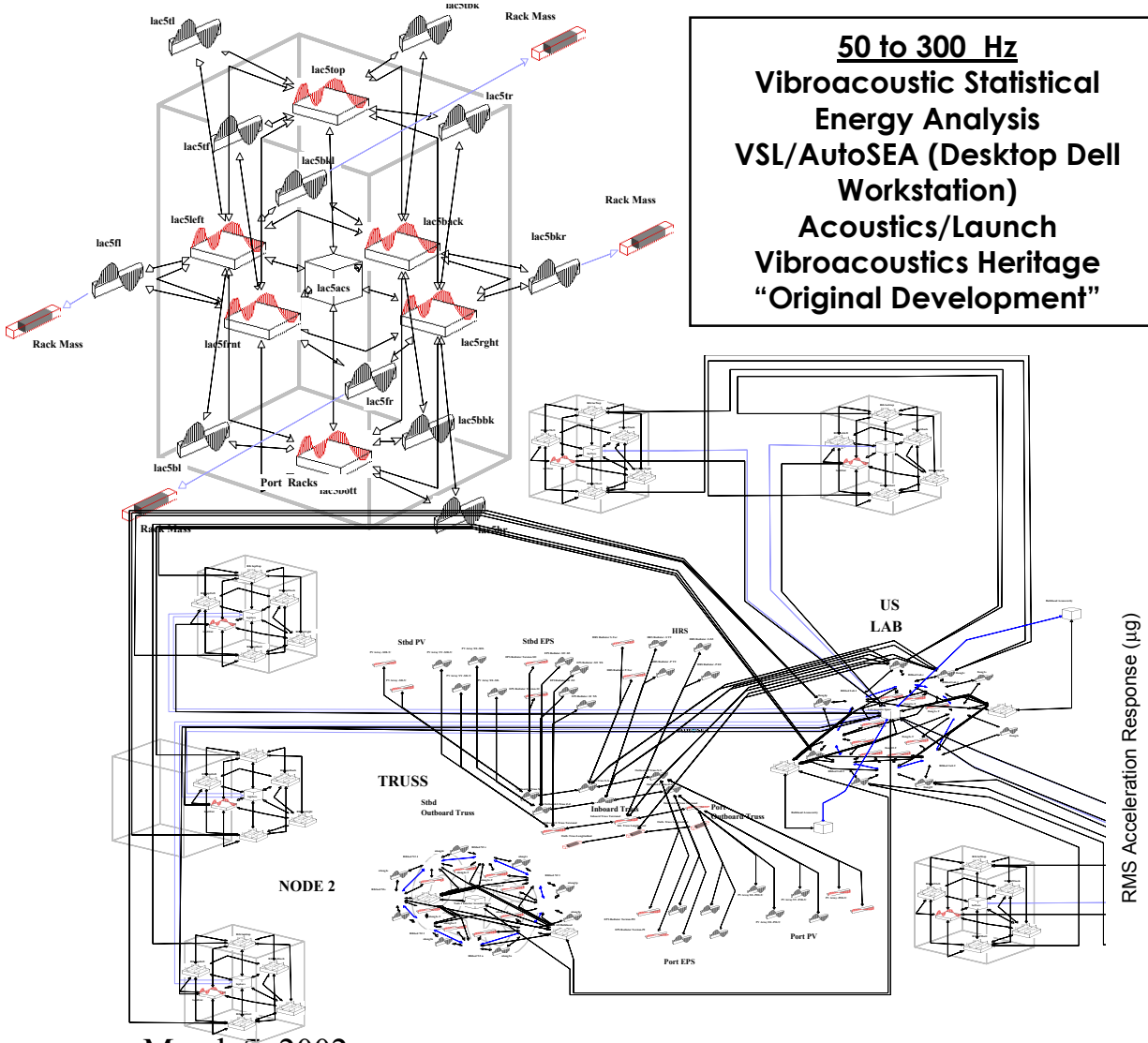
Upper KBAR

Rack KBAR Attachment

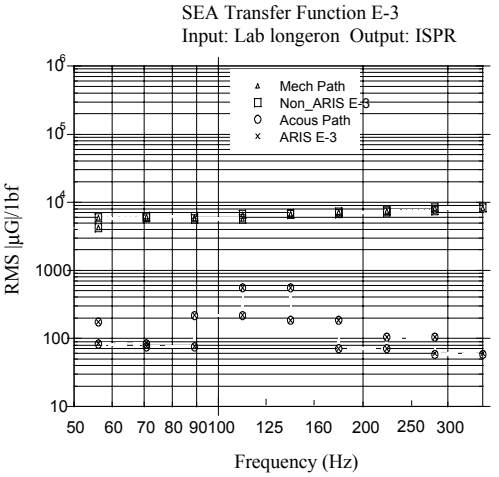


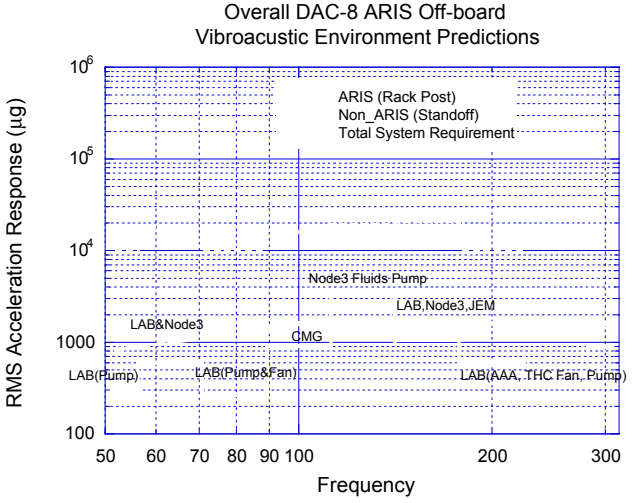


Methods & Tools
VibroAcoustic Analysis

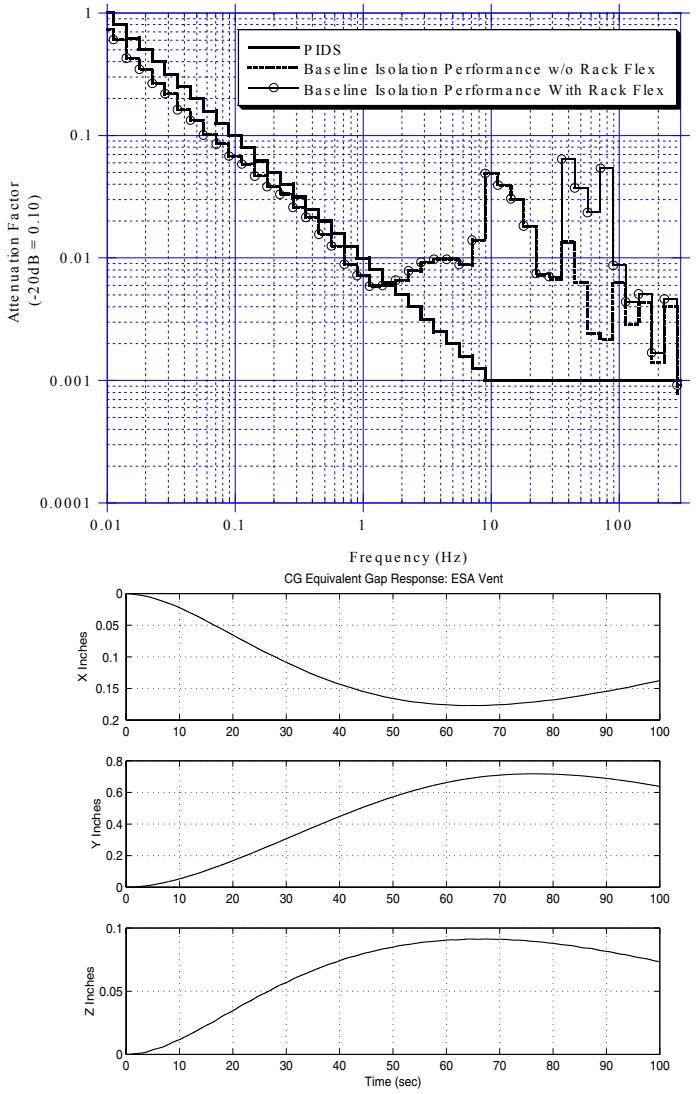


50 to 300 Hz
Vibroacoustic Statistical Energy Analysis
VSL/AutoSEA (Desktop Dell Workstation)
Acoustics/Launch Vibroacoustics Heritage
"Original Development"

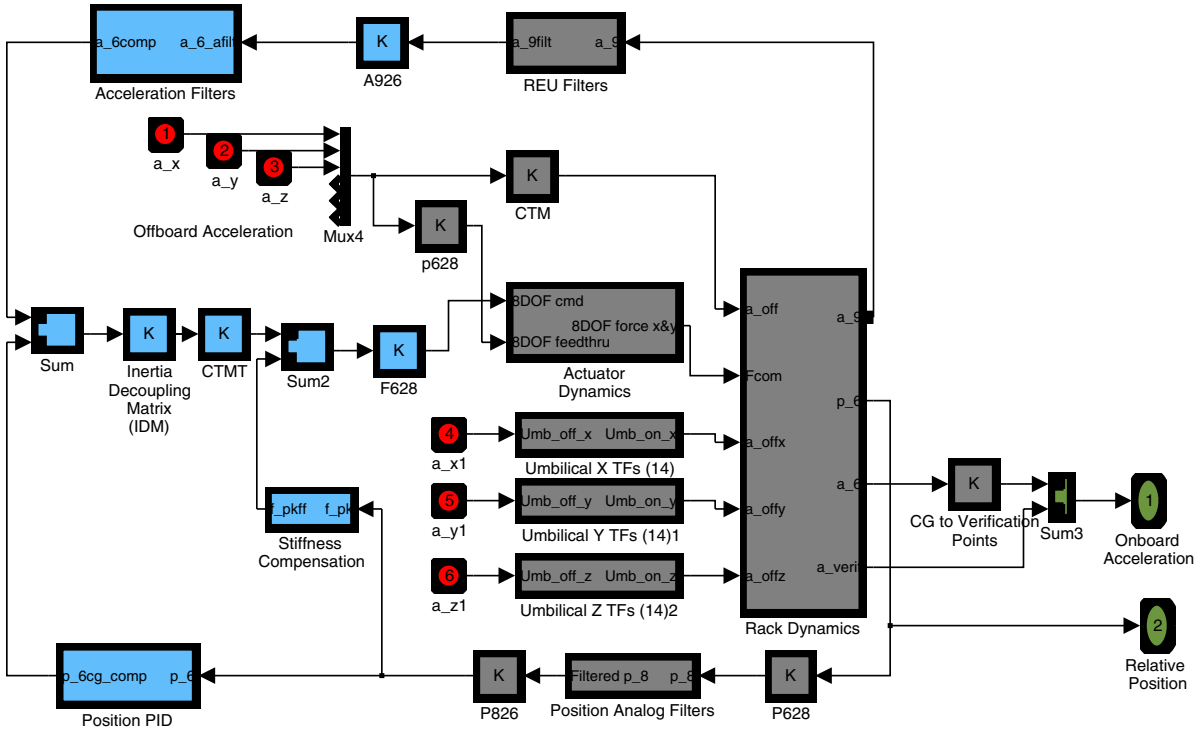




Methods & Tools
Controls Analysis

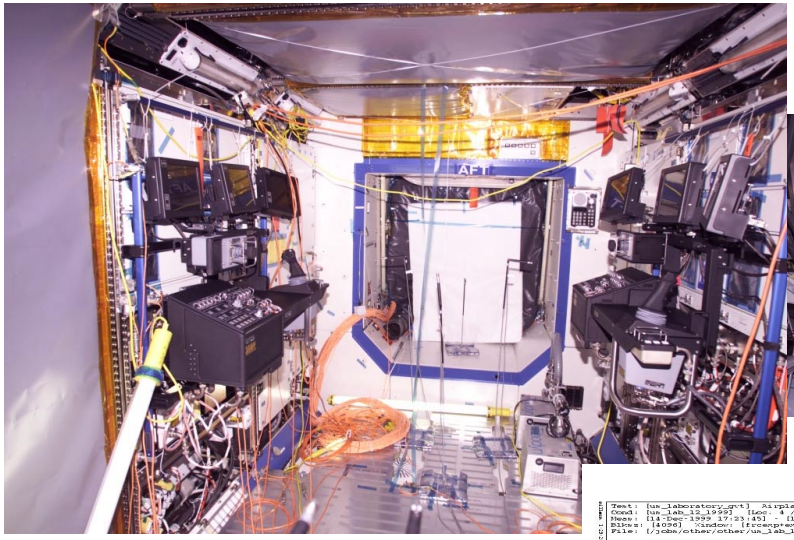


Active Rack Isolation System
Control System Analysis
Matlab/Simulink (NASASparc)

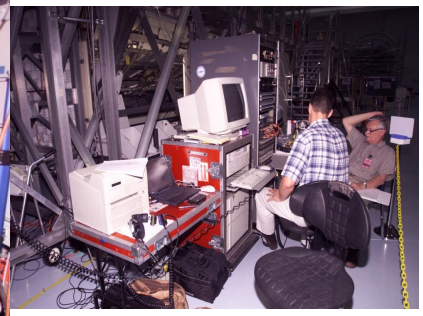


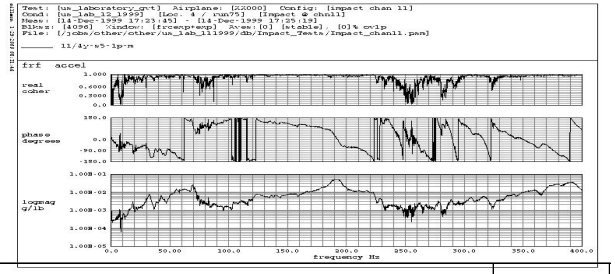
Methods & Tools
Disturbance Analysis & Testing

NODE TEST



LAB TEST



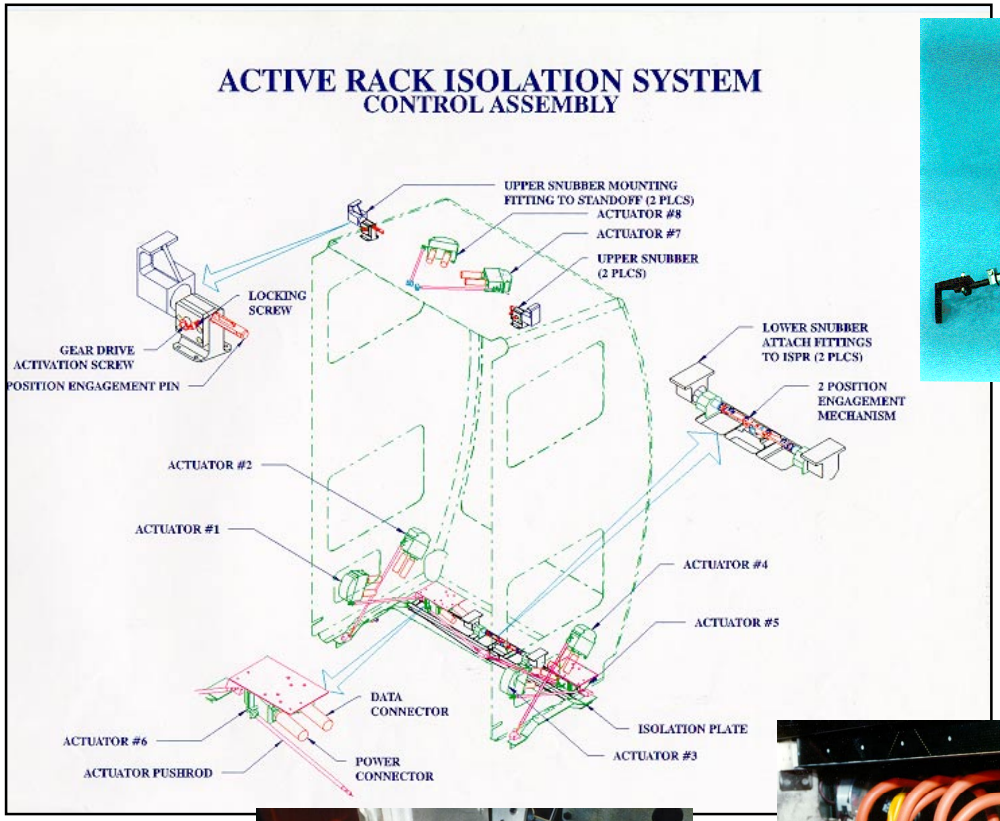


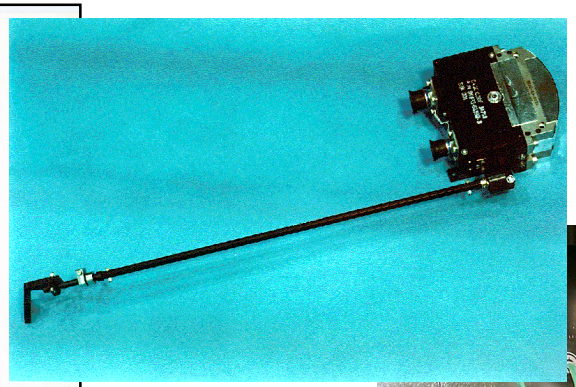
EQUIPMENT							
TYPE	ITEM	DAC5 VMDB	RSA ORU LOGISTICS	KhSC EN-10-01, P2	PRIME DDB	COMMENTS	ASSESSED
SOLAR ARRAY	DRIVE	1	2	2	2		
FAN	THC	2	11	8	8	VIB ONLY	X
	DUST COLLECTOR			2	2	VIB ONLY	X
	CONTROL SYSTEM			1	1	NQ	N/A
	CONTIN. FILTER			1	1	NQ	N/A
	TCS			2	2	1-VIB, 1-NQ	1-X, 1-N/A
	COMFORT	1	3	3	3	LOW POWER	N/A
	FIRE HAZARD			10	10	LOW POWER	N/A
	BANK OF FANS	1					
	LIFE SUPPORT	1	4				
PUMP	TCS	2		2	2	VIB ONLY	X
HEAT EXCH.	TCS - GAS/LIQUID	2		4	4	KHSC INSIG.	
VALVE	TCS RETURN	1		2	2	KHSC INSIG.	
	TCS REGULATOR	1		1	1	KHSC INSIG.	
	LIFE SUP-PRESS	1		1	1	KHSC INSIG.	
	LIFE SUP-PRESS REDUCTION	1		1	1	KHSC INSIG.	
	LIFE SUP-EQUAL	1		1	1	KHSC INSIG.	
	LIFE SUP-CNTRL	2		1	1	KHSC INSIG.	
TV	CAMERA	1		3 EXT-NQ	3 EXT-NQ	EXT & NQ	N/A
PHONE	LOUDSPEAKER	3	4	3	3	CONTINGINCY	N/A
TOTAL		22	24	45	45		

Capture & Adequacy

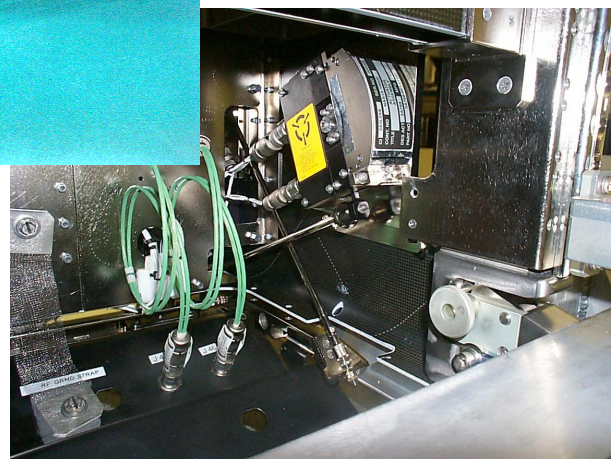
EQUIPMENT			PG/IP	DISTURBANCE COMPONENT ASSURACY (WEIGHTING * RATING)								ACCURACY RATING
TYPE	ITEM	NUMBER		QUASI-STEADY		VIBRATORY						0 </= AR </= 10
						MECHANICAL				ACOUSTICAL		
						NB		WB	TR	NB	WB	TR
						Fndmtl.	Harmonics			Fndmtl.	Harmonics			
Flight 1A/R - FGB												
	ECLSS Fans	12	RS			8*8	4*8	2*0			1*0		6.4
	TCS Pumps	2	RS			8*6	4*6	2*0			1*0		4.8

ARIS

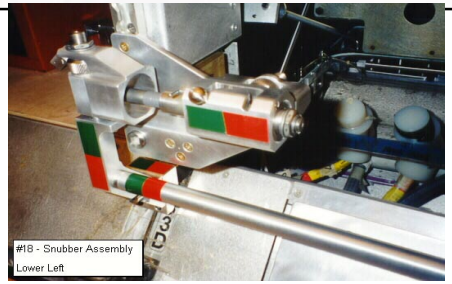




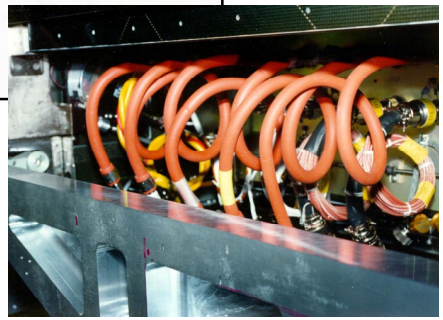
Actuator



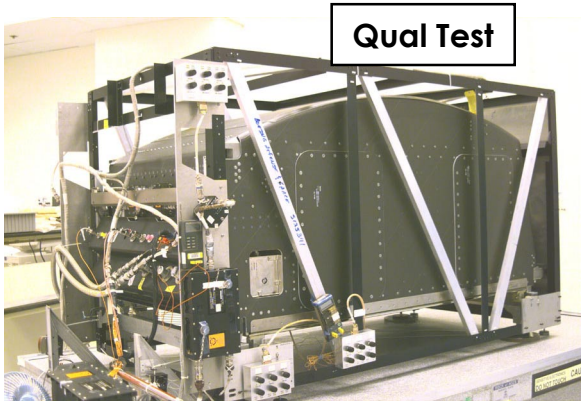
Qual Test



Snubber



Umbilicals



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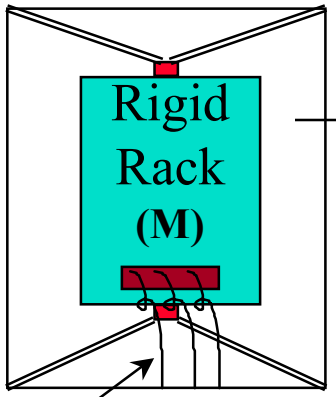
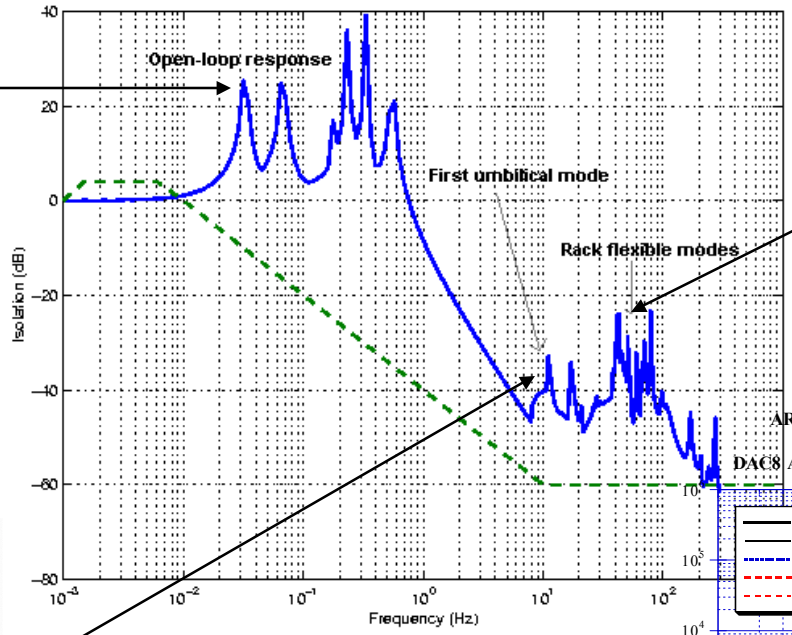
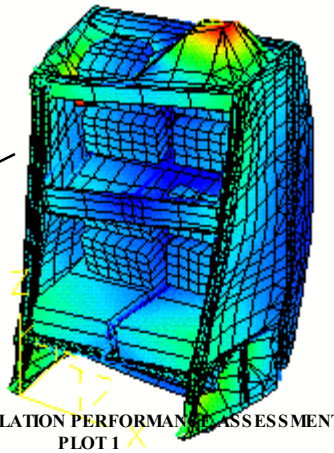
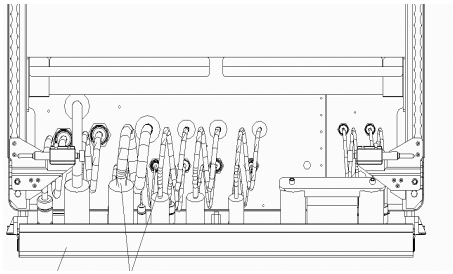


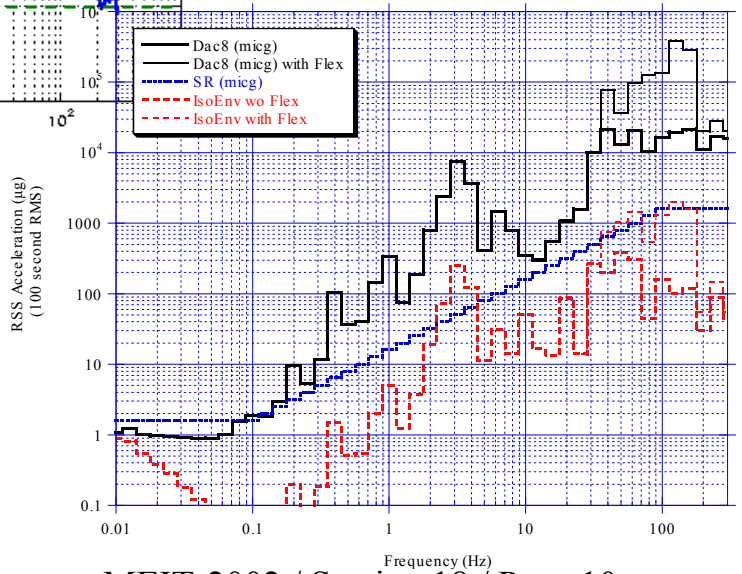
Umbilicals (K)







ARIS FCA/PCA ISOLATION PERFORMANCE ASSESSMENT
PLOT 1
DAC8 Acceleration Environment With & Without Rack Flex Effects

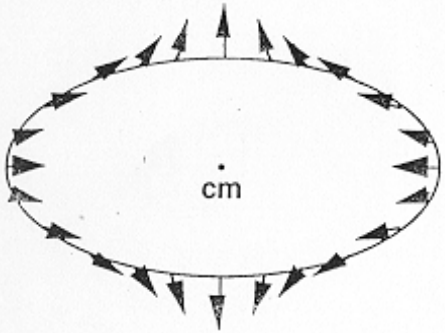


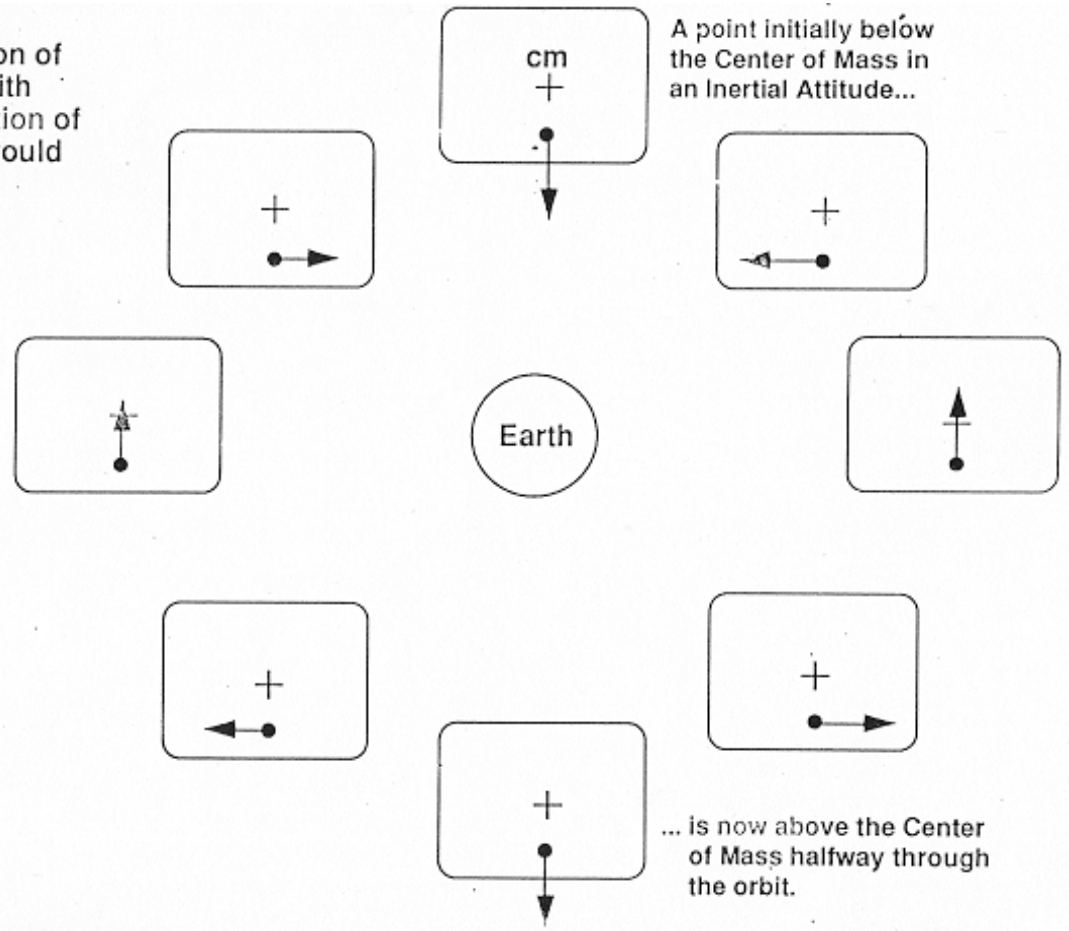
- **Resonances between 0.01-1 Hz are rigid rack-umbilical modes (M-K)**
- **Resonance around 10 Hz is the umbilical loop resonance**
- **Resonances above 26 Hz are due to rack flexible modes being excited by umbilical and pushrod resonances.**

Forcing Functions
Quasi-steady Stability - Once Per Orbit Rotation

In an inertial attitude, the orientation of a point on a body would change with respect to Earth; hence, the direction of the gravity gradient acceleration would change with respect to the body.

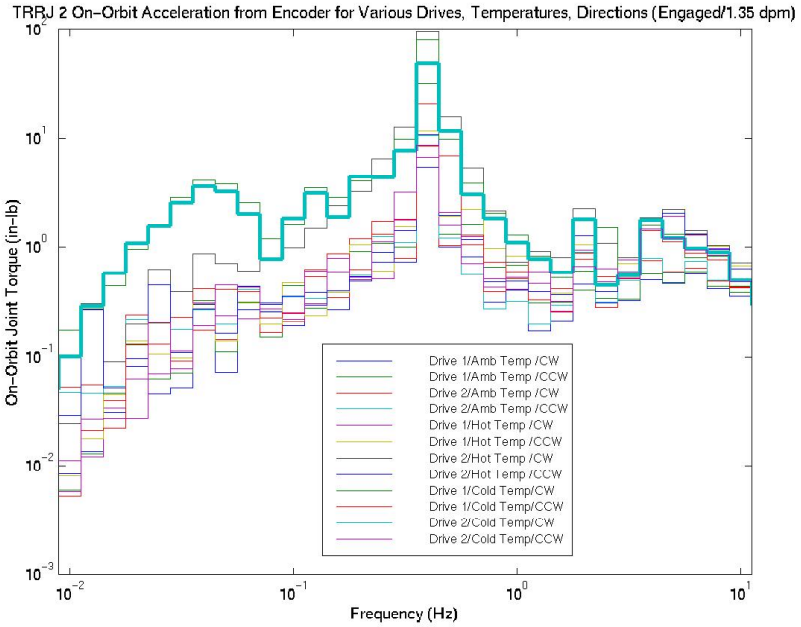
Recall the Gravity Gradient Ellipsoid

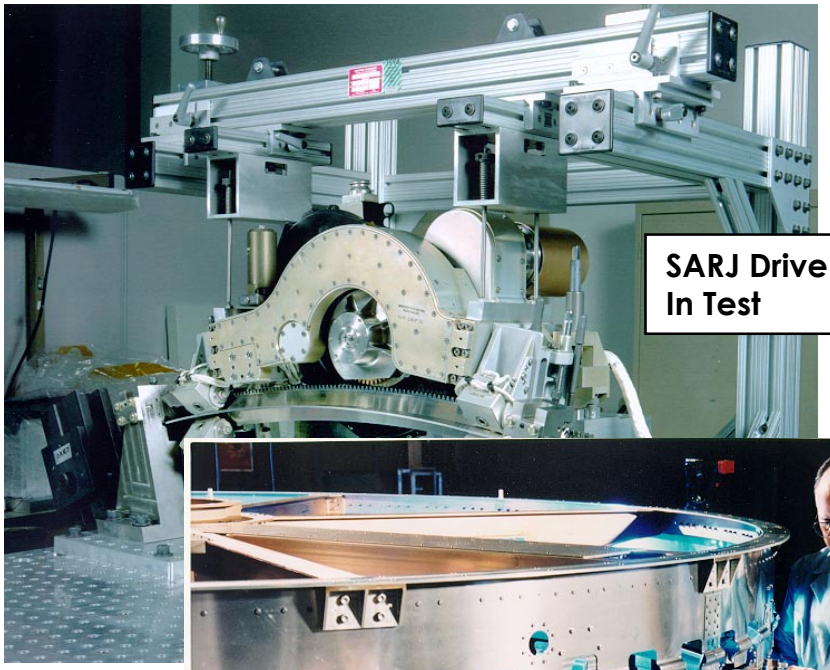




Forcing Functions
Articulate Joints For PV Array Solar Incidence

Solar and Radiator Rotary Joints: Torque Ripple, Bearing Friction, Gear Train Meshing Friction, Position/Resolver Error

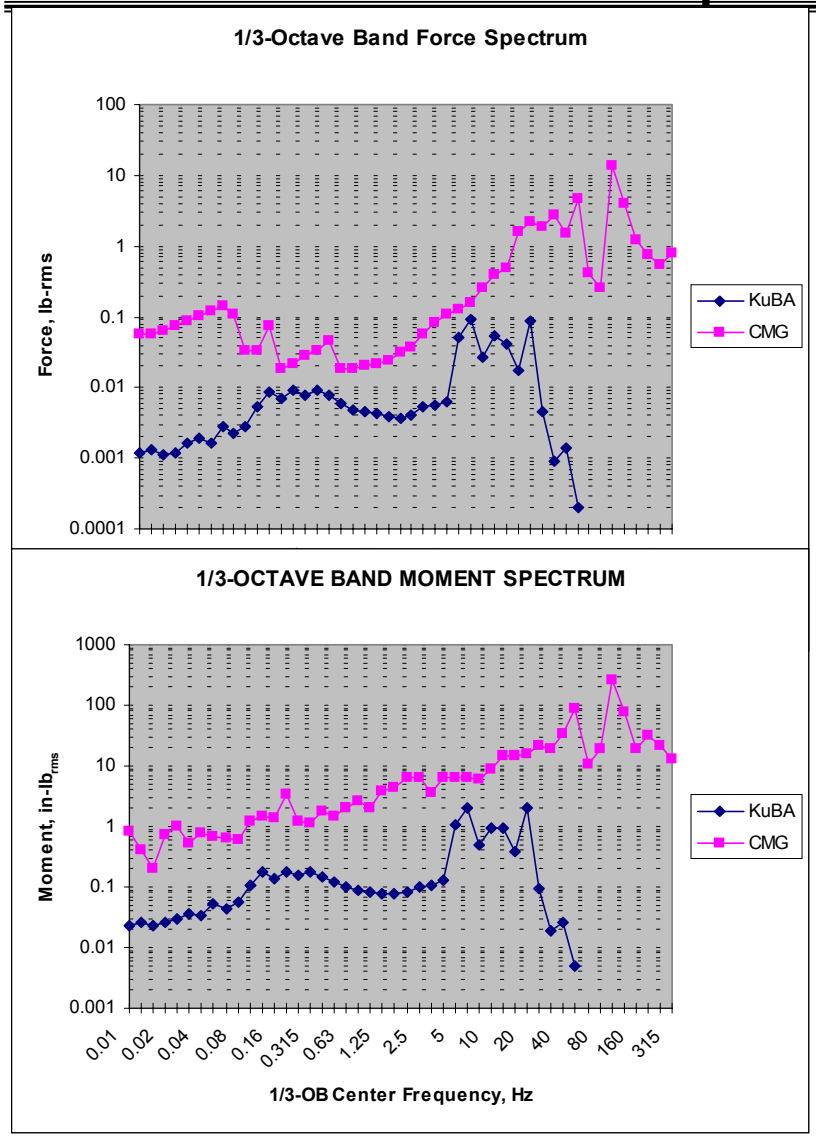


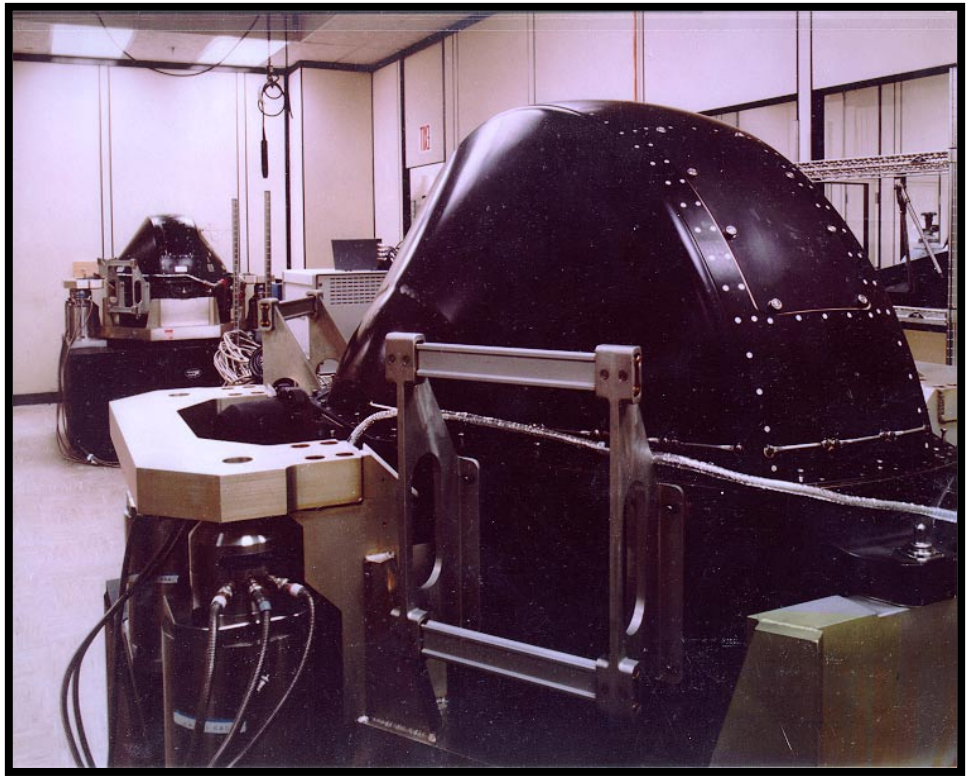


SARJ Drive Motor In Test

SARJ Qual Unit With Trundle Bearings Installed

Forcing Functions Control Moment Gyros For Torque Equilibrium Attitude

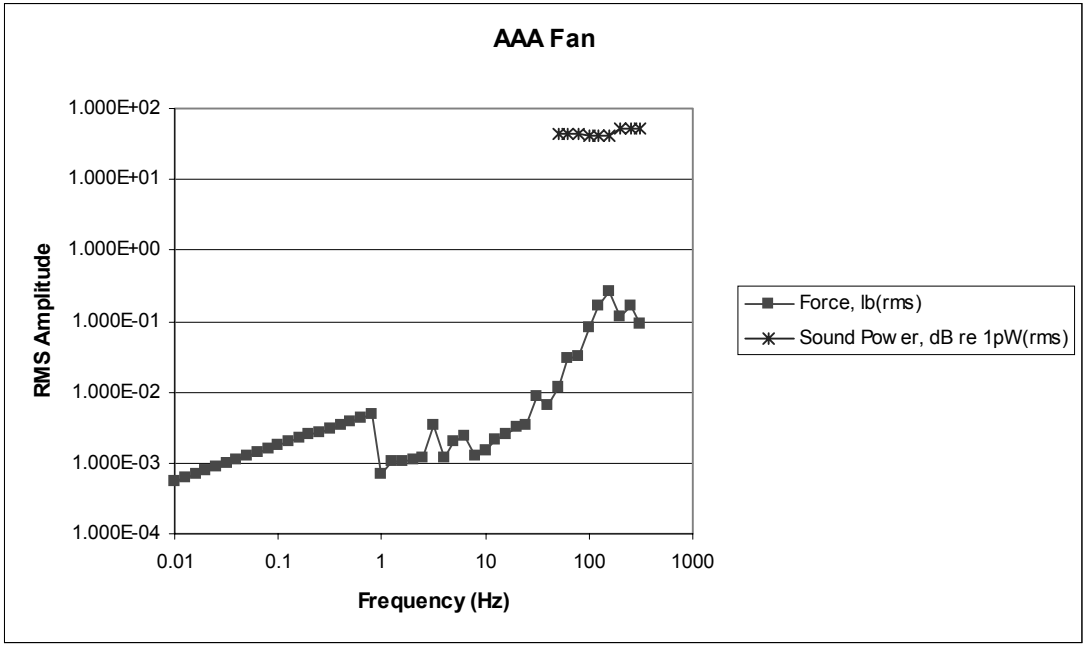




Co. / Agency	BHV			
Item	Fan, AAA (175 W, nominal)			
Location (Number)	(1), (17), (32), (13), (5), (14), (1), (16), (4), (2), (1), Lp4 (1)			
Duty	0.2 for each fan			
References	144			
Bibliography	1,2,11,17,26,38,50,52,55,56,75			
Comments	Unbalance force is assumed to be 0.115			
1/3-OB Ctr Freq, Hz	Time, s	Force, lb(rms)	Moment, in-lb(rms)	Sound Power, dB re 1pW(rms)
0.01		5.520E-04		
0.0125		6.175E-04		
0.016		6.960E-04		
0.02		7.810E-04		
0.025		8.730E-04		
0.0315		9.820E-04		
0.04		1.100E-03		
0.05		1.235E-03		
0.063		1.390E-03		
0.08		1.560E-03		
0.1		1.750E-03		
0.125		1.950E-03		
0.16		2.200E-03		
0.2		2.470E-03		
0.25		2.760E-03		
0.315		3.100E-03		
0.4		3.490E-03		
0.5		3.910E-03		
0.63		4.380E-03		
0.8		4.940E-03		
1		6.995E-04		
1.25		1.033E-03		
1.6		1.033E-03		
2		1.113E-03		
2.5		1.212E-03		
3.15		3.497E-03		
4		1.194E-03		
5		2.034E-03		
6.3		2.373E-03		
8		1.288E-03		
10		1.525E-03		
12.5		2.159E-03		
16		2.498E-03		
20		3.200E-03		
25		3.321E-03		
31.5		8.471E-03		
40		6.464E-03		
50		1.197E-02		4.450E+01
63		2.921E-02		4.450E+01
80		3.200E-02		4.450E+01
100		8.052E-02		4.120E+01
125		1.643E-01		4.120E+01
160		2.564E-01		4.120E+01
200		1.155E-01		5.200E+01
250		1.633E-01		5.200E+01
315		9.077E-02		5.200E+01

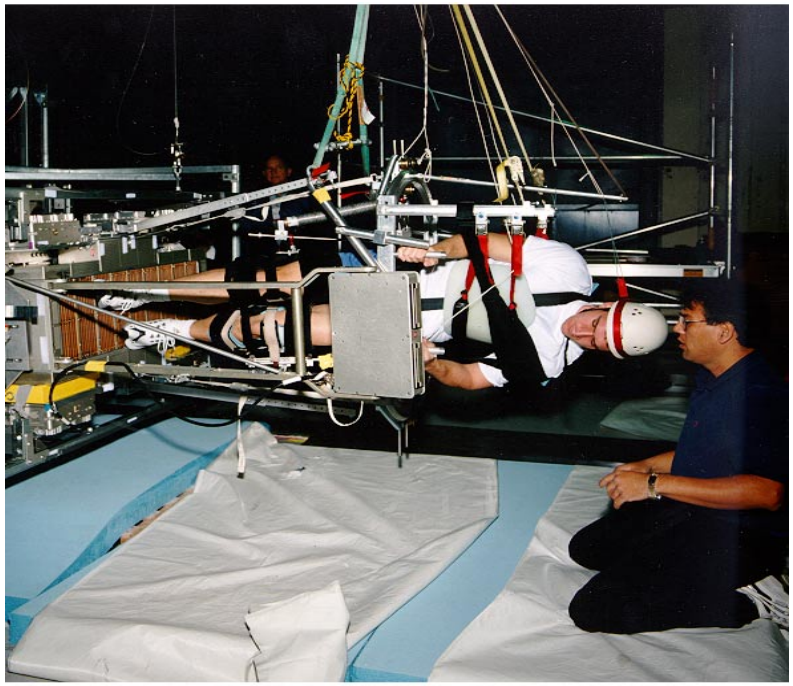
DISTURBANCE DATABASE

<u>Pressurized Module Disturbances:</u> Fans, Pumps, Valves, Coldplates, Ducts (Mechanical and Acoustic)

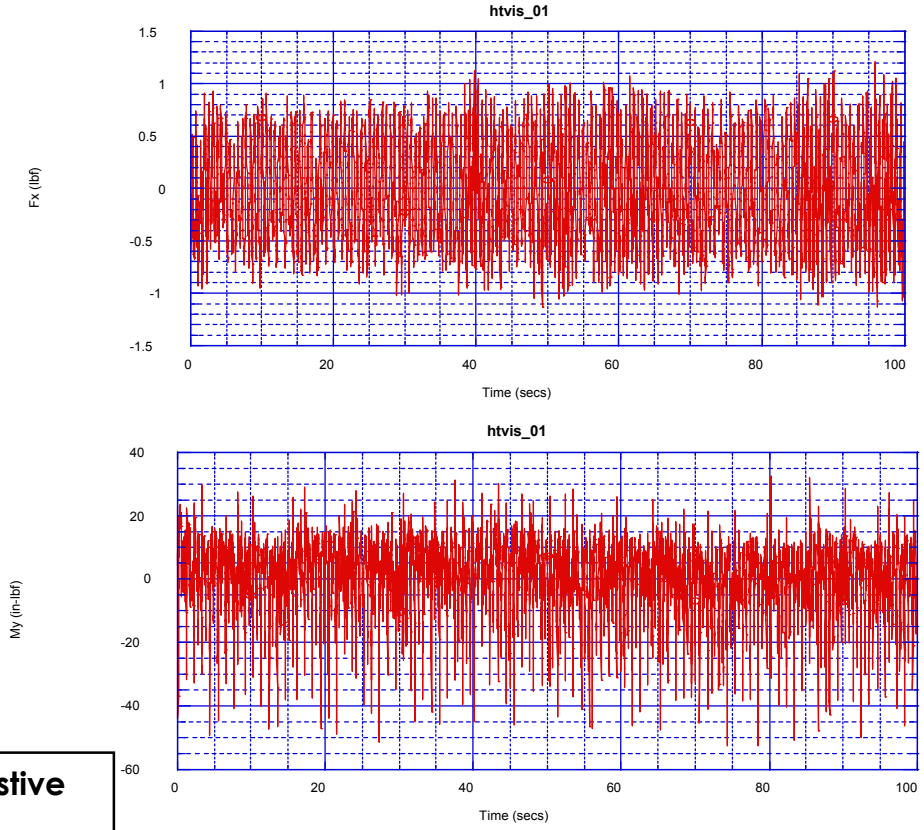


Forcing Functions

TVIS Certification Test



6 DOF Transient Force/Moment For Various Subjects



Crew Exercise Equipment: Treadmill, Ergometer, Resistive Exercise Device (Isolated/Non-isolated)

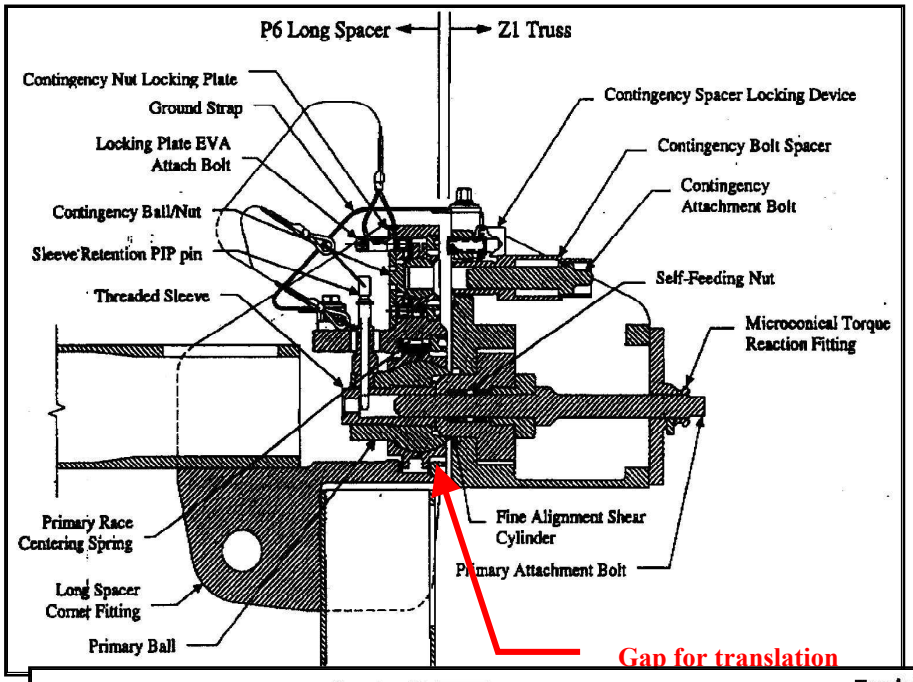
InterVehicular Activity: Translation, Station Keeping, Console Operations, … Scheduled Maintenance.

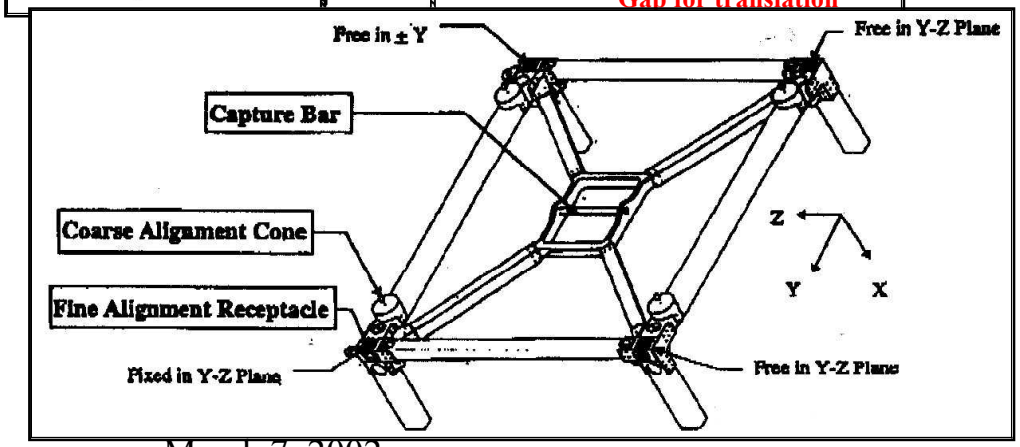
Forcing Functions

Thermal Induced Vibration

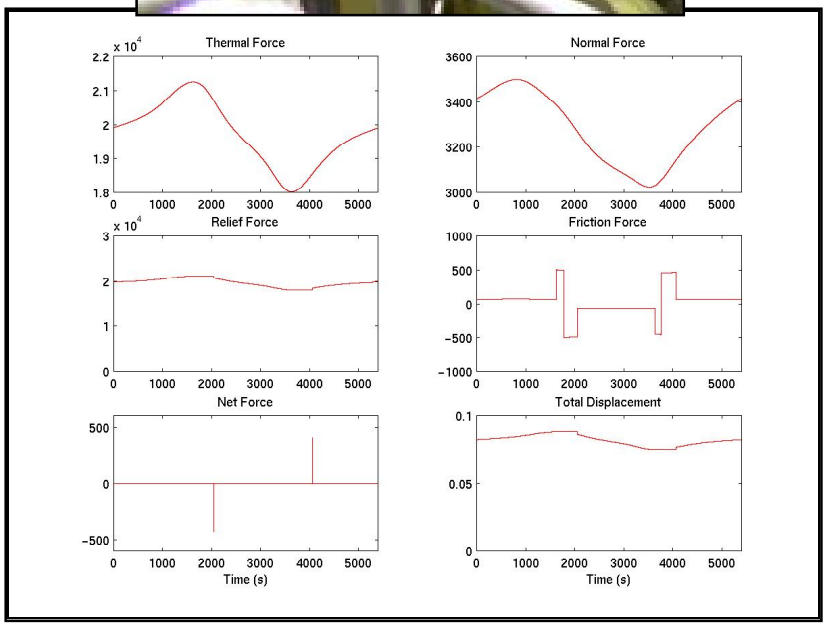
HARDWARE ITEM	STATIC FRICTION RELEASE (STICK-SLIP)	THERMAL STEP & MODAL DEFLECTION	SLOWLY VARYING DEFORMATION (~ORBITAL RATE)	THERMAL BUCKLING (OIL CANNING)
SHORT SPACER/ LONG SPACER INTERFACE	SIGNIFICANT • Rocketdyne Truss Attachment System (RTAS) forcing function developed by BHB (Refs. 10, 11, & 12). • BHOU assessment indicates that RTAS stick/slip is a Microgravity Critical Item (MGCIL) (Refs. 4). • Disturbance adequacy rating of 7 meets verification criteria.	NOT APPLICABLE TO INTERFACE	NOT APPLICABLE TO INTERFACE	NOT APPLICABLE TO INTERFACE
LONG SPACERS	NONE • No sliding joints other than at interface with short spacer – see short spacer/long spacer interface (Ref. 6).	NONE • No vibration modes below 30 Hz (Ref. 6).	NOT APPLICABLE • Item by itself is very stiff. Only when integrated with other elements (including non-PG2) will item experience low frequency motion (Ref. 17).	NONE • Constructed of hollow, extruded aluminum tubes with 3/16 inch minimum thickness. There are no thin plates or long slender members(Ref. 6).
IEAs	NONE • No sliding joints other than at interface with EPS radiator (Ref. 6) – see IEA/EPS radiator interface.	NONE • No vibration modes below 30 Hz (Ref. 6). • An IEA with full sun exposure could see a heat-up rate of 4 degrees F per hour. The rate is slow due to the mass of the structure (Ref. 20).	NOT APPLICABLE • Item by itself is very stiff. Only when integrated with other elements (including non-PG2) will item experience low frequency motion (Ref. 17).	NONE • Free thermal expansion with no thin plates or long slender members (Ref. 6)
EPS RADIATORS	NONE • No sliding joints other than at interface with EPS radiator (Ref. 6) – see IEA/EPS radiator interface.	NEGLIGIBLE • Fundamental vibration mode at 0.23 Hz is too high to be affected by slow temperature variations (Ref. 6). • Other than the PV Arrays, most items have a long thermal time constant, e.g. 15 minutes for the radiators (Ref. 15). • Each radiator weighs about 1600 lbs, compared to 2400 lbs for the PV Array, and about half of it is a concentrated load at the base. The radiator is about a quarter of the size of the PV Array. The forces and moments generated at the base of the radiator will be much smaller than that generated at the base of the PV Array which are negligible (Ref. 17).	NEGLIGIBLE • Each radiator weighs about 1600 lbs, compared to 2400 lbs for the PV Array, and about half of it is a concentrated load at the base. The radiator is about a quarter of the size of the PV Array. The forces and moments generated at the base of the radiator will be much smaller than that generated at the base of the PV Array which are negligible (Ref. 17).	NONE • The radiators are freely expanding structures (Refs. 6 & 17).

Forcing Functions

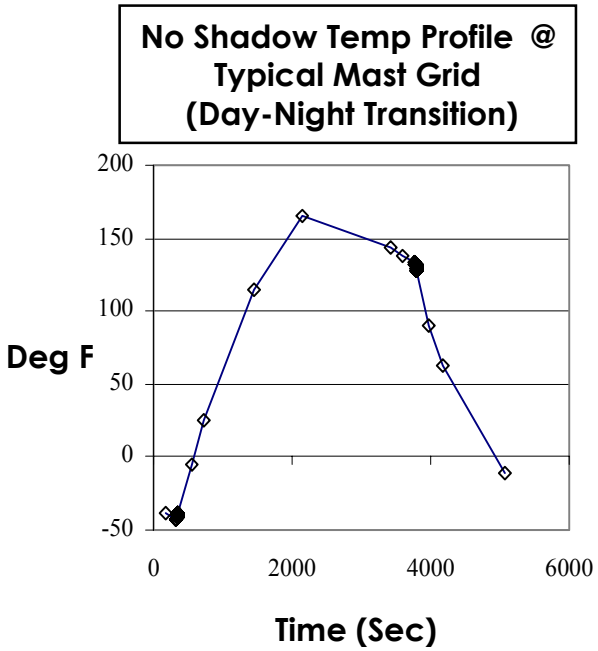




RTAS Stick-Slip

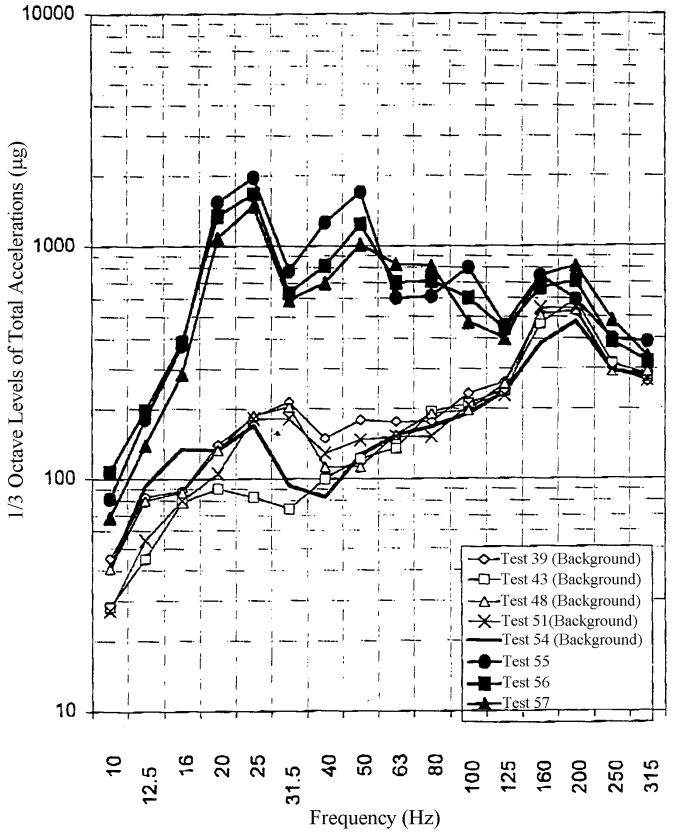


Forcing Functions



Forcing Functions

RS Service Module Element Ground Test



ESA Columbus Module Component Ground Test

ECLSS : -

* one Cabin fan assy (CFA EM5) (test data eq. &sect.)
* one Cabin fan assy as IMV Supply fan (test data eq. & sect.)
* one Cabin fan Assy as IMV Return Fan (test data - eq. &sect.)
* two Condensate Water Separator Assies (CWSA EM) (test data - eq. & sect.)
* one Condensate Heat Exchanger/Thermal Control valve (CHX/TCV) (testdata - eq. & sect.)
* TWO WASTE GAS Line shut Off Valve (LSOV) (test data -eq.)
* One WLSV EM (test data - eq.)
* Two PPO2 (test data -eq.)
* Airbox (Test data-Section)

TCS:

* one WPA (test data -eq.))
* one WOO (actuated) (test data -eq.)
* two WTMO (actuated) (test data - eq.)
* fluxed ducting (test data - sect.)

Structural Stick/slip :

* Stick/slip at MDPS/bracket interface (analytical evaluation)

NASDA ICS Antenna Slew & Tracking

ISS Traffic Model

- The traffic plan includes a complete traffic event schedule and a projected resupply/return loading by cargo category starting with first element launch through end of life.
- The integrated traffic plan is also used to support design analysis, unique transportation system studies, off-nominal operations planning, and to assess the viability of long-term planning inputs from International Partners.

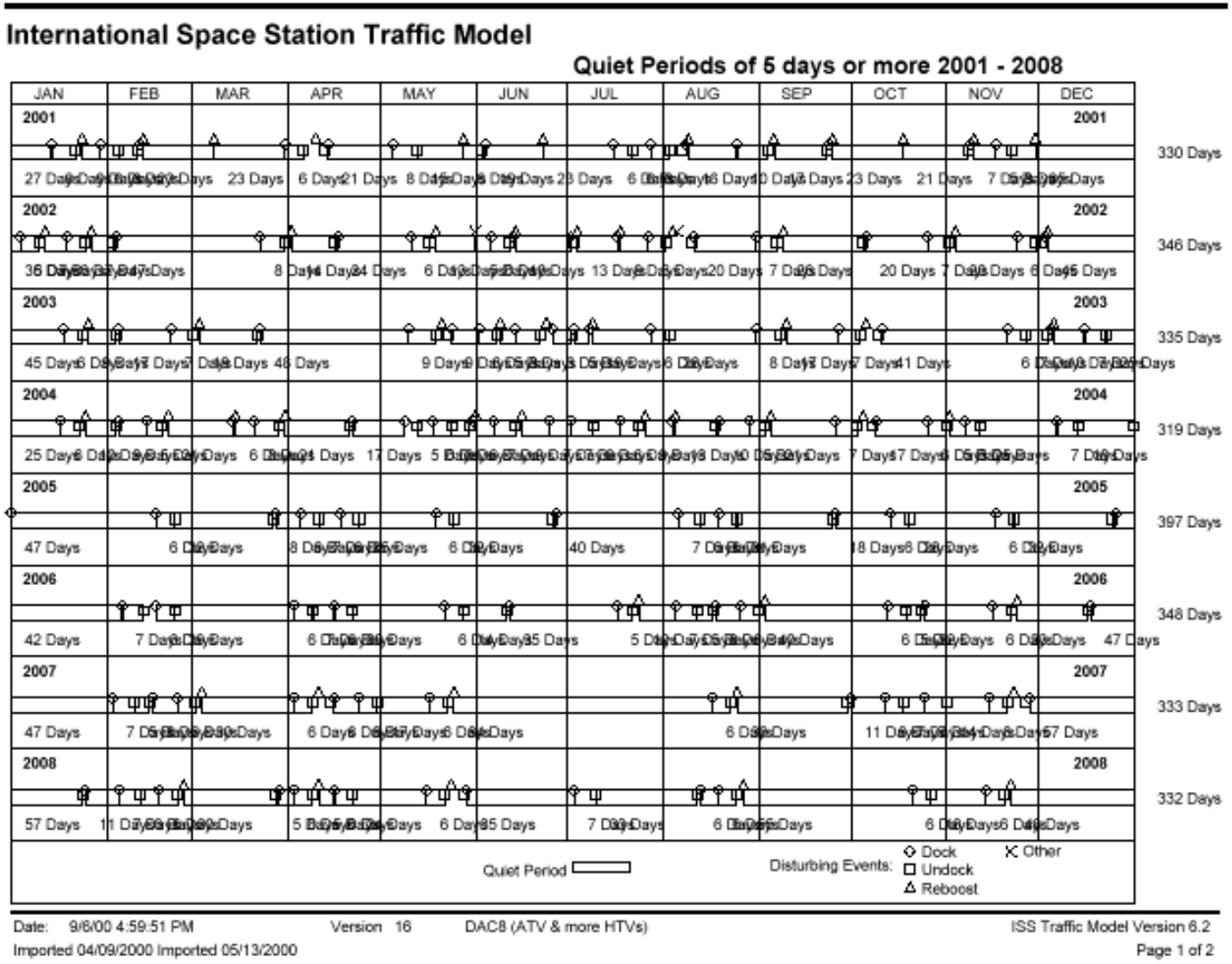
What are the major disturbers to ISS micro-g

- Docking events
- Undocking events
- Reboosts
- EVAs

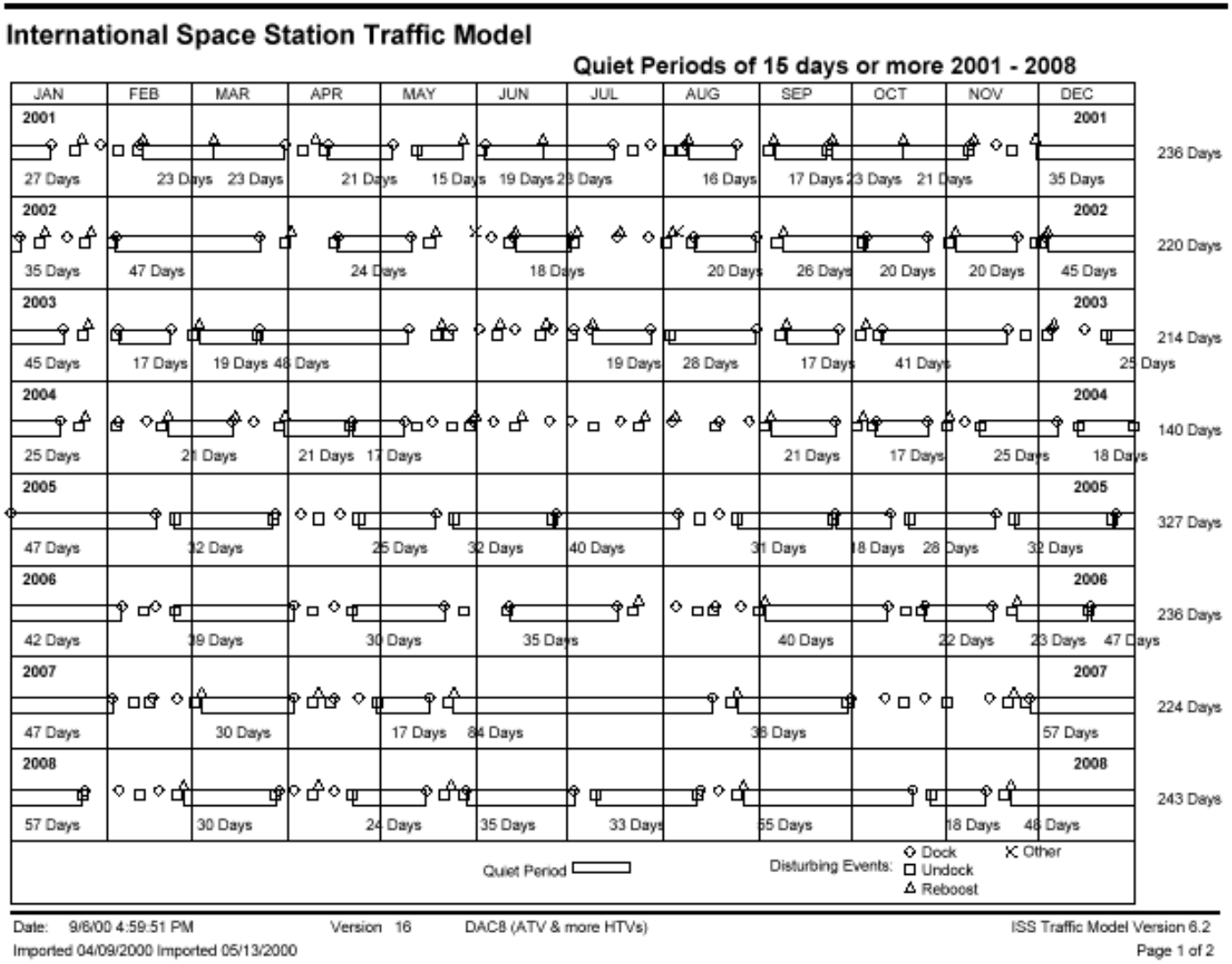
Threats to micro-gravity periods

- Debris Avoidance Maneuvers
- Deferred or contingency EVAs
- Launch schedule changes

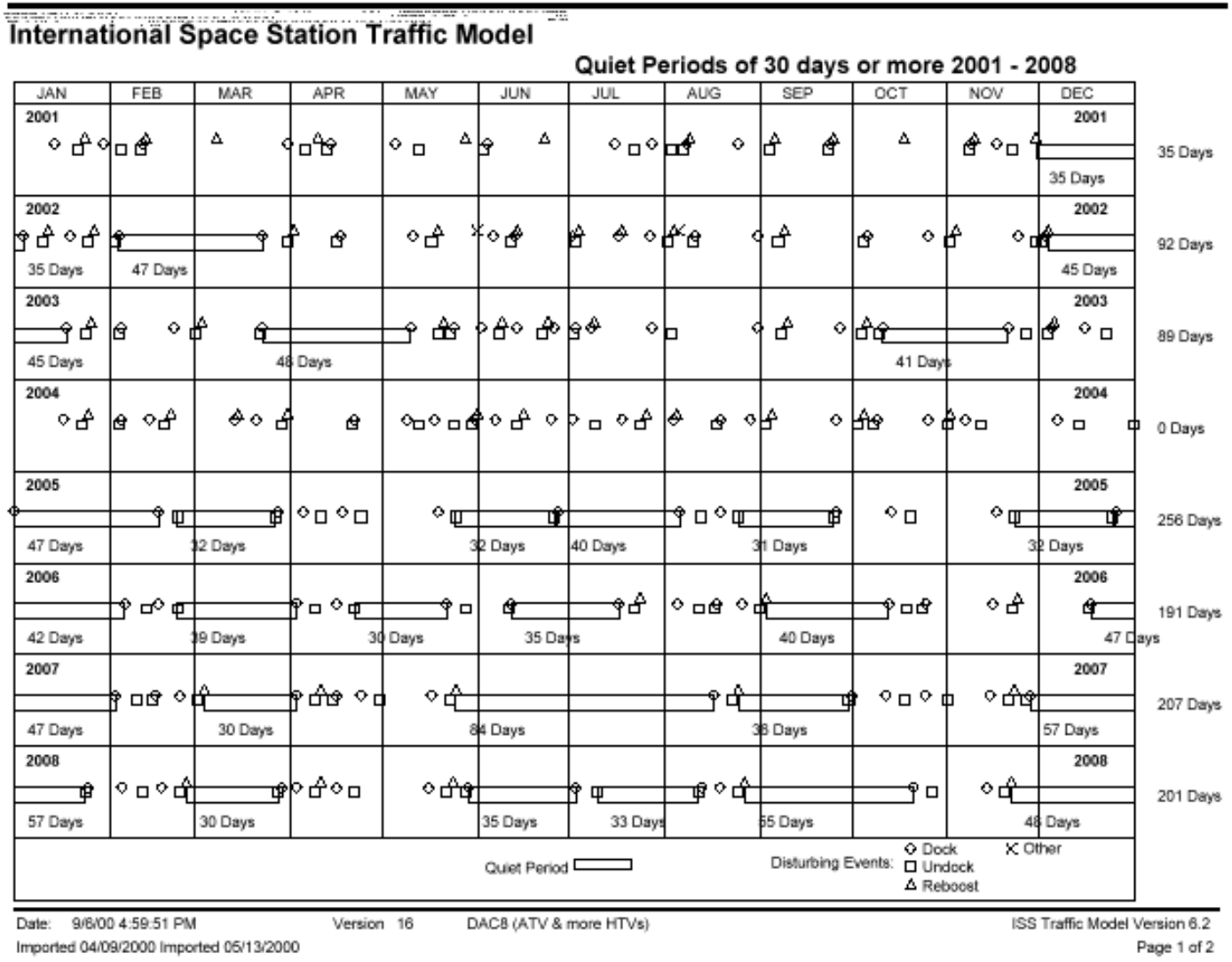
DAC8 Assembly >5 Day Periods



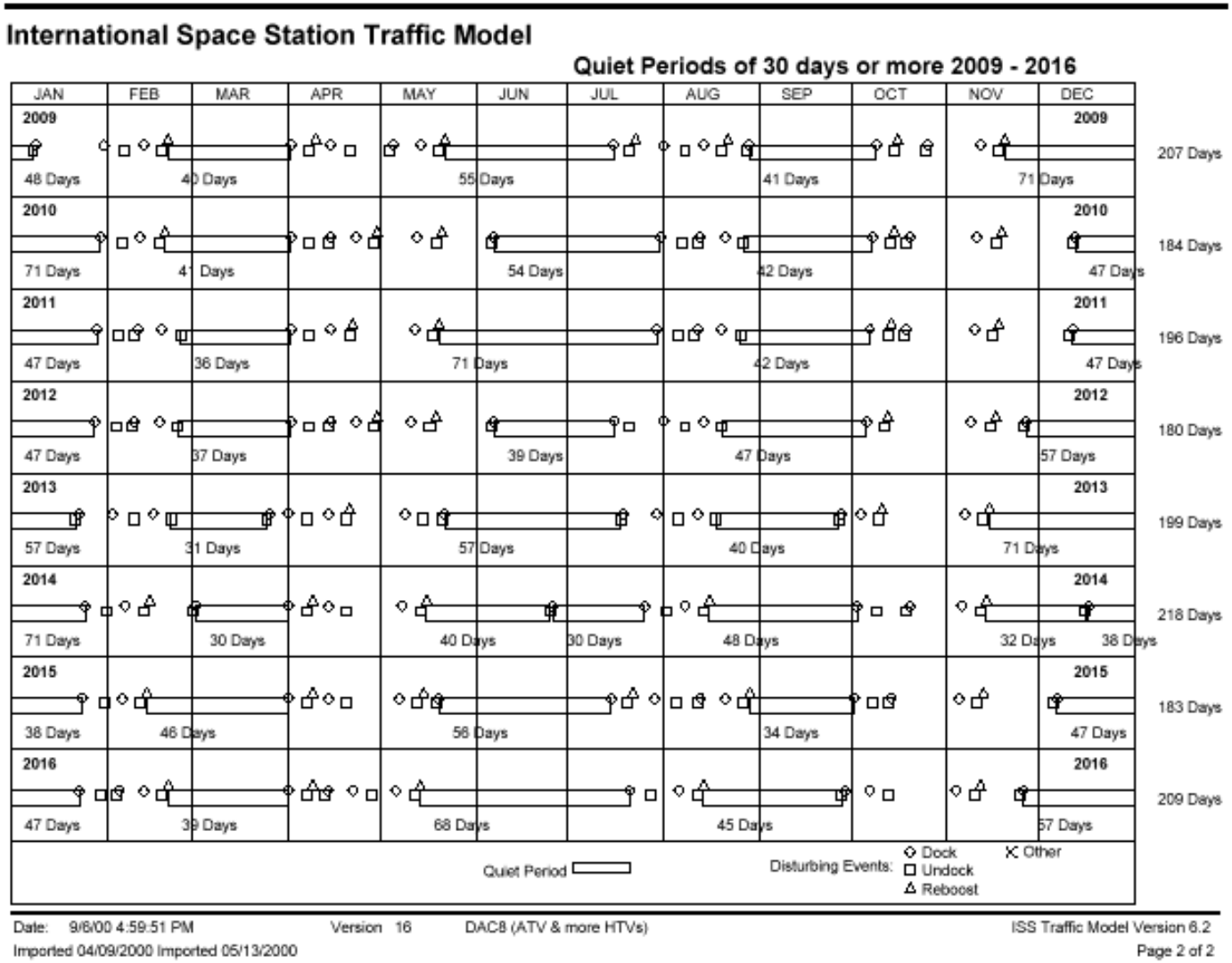
DAC8 Assembly >15 Day Periods



DAC8 Assembly >30 Day Periods



DAC8 Assembly Complete >30 Day Periods

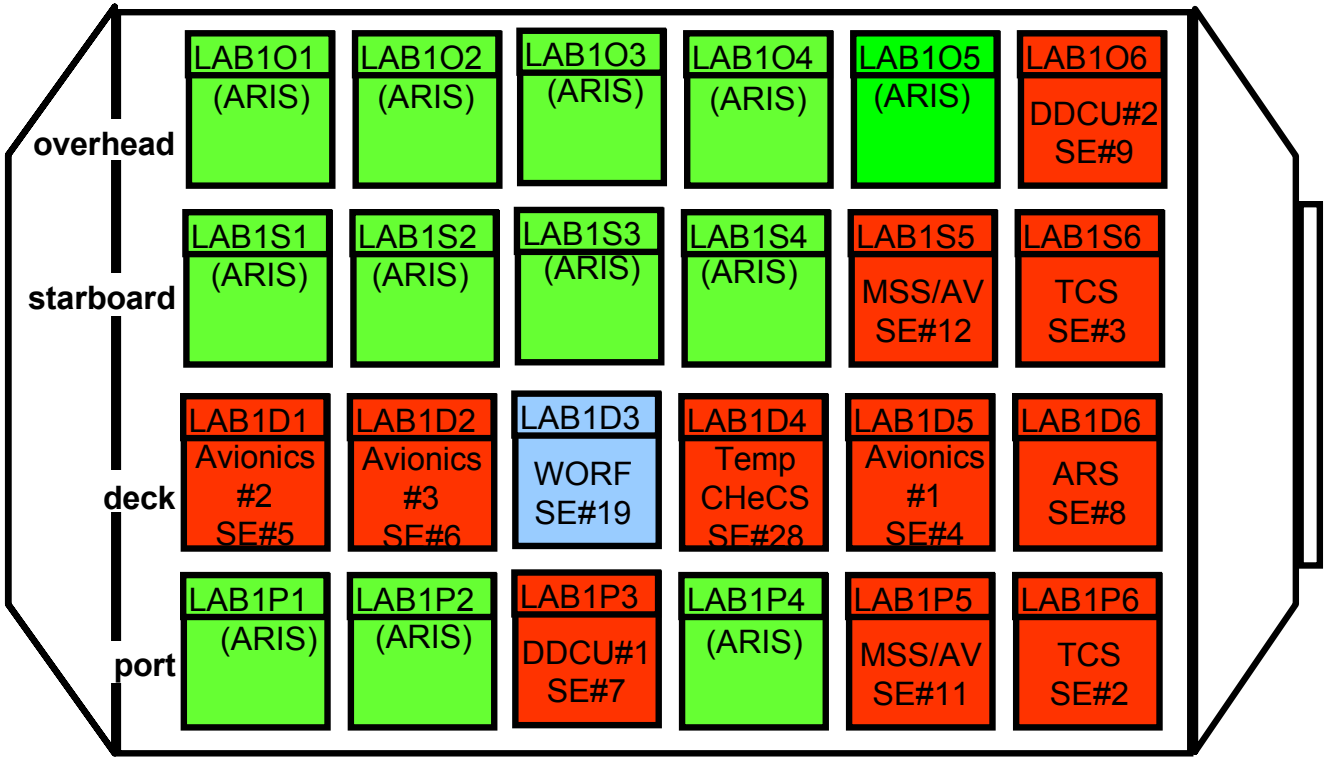


Conclusion

- **Currently there is no requirement to meet the micro-gravity period requirement during assembly**

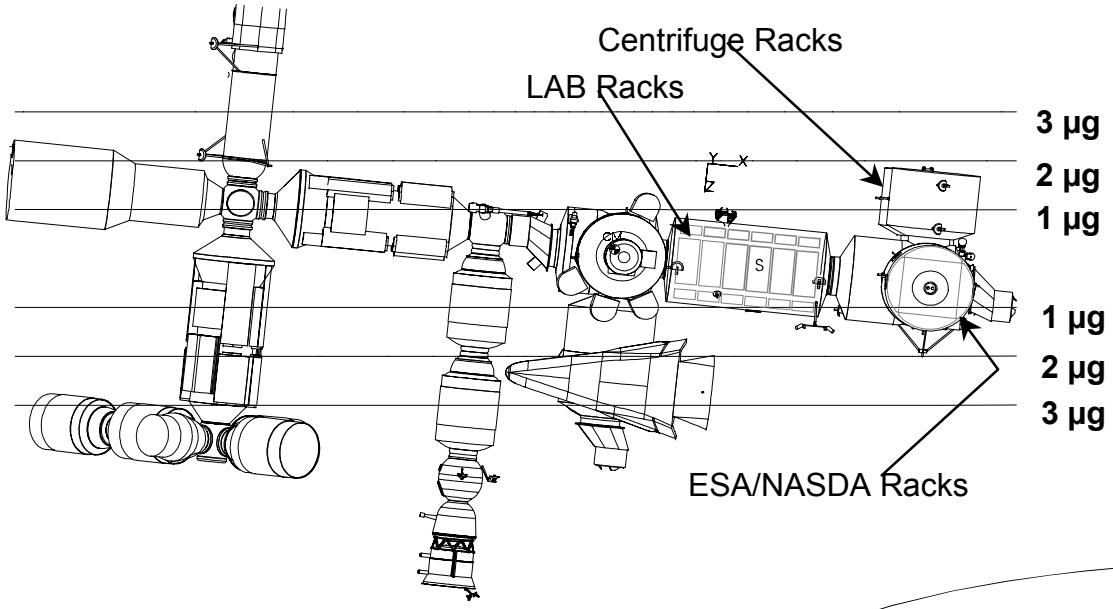
- **Based on analysis the micro-gravity requirement can be satisfied during the assembly complete period**

Rack Topology at Assembly Complete (Analysis Configuration)

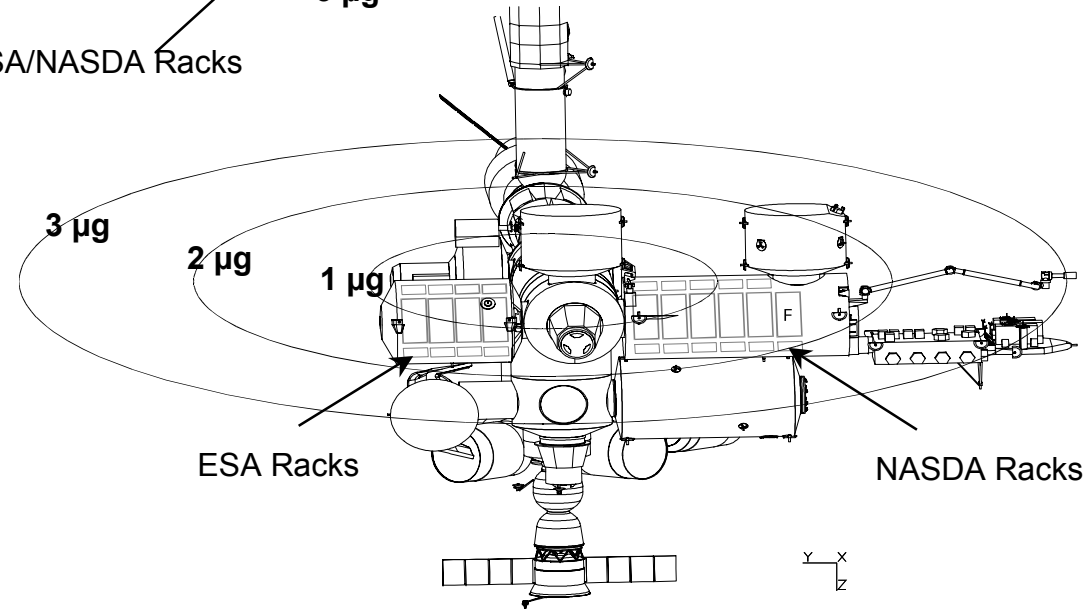


System Rack Payload Rack Payload Rack (Non-ARIS)

DAC8 Quasi-Steady Performance



Quasi-steady Performance:
- **15 of 32 ISPRs < 1.0 µg**
- **16 of 32 ISPRs < 1.2 µg**
- **All satisfy stability criteria**



Flight Attitude:
- **Pitch -6.97 degrees**
- **Yaw -8.07 degrees**
- **Roll 1.16 degrees**

DAC8 Quasi-Steady Performance

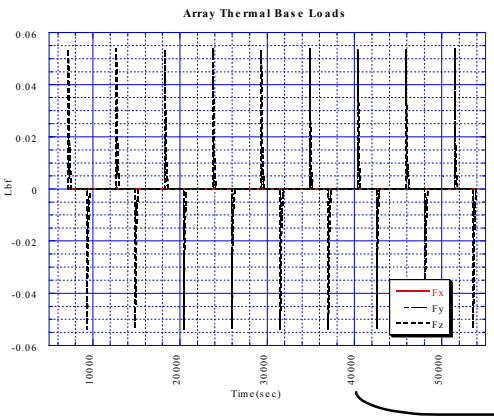
15 of 32 racks less than 1 μg magnitude & 0.2 μg perpendicular component.

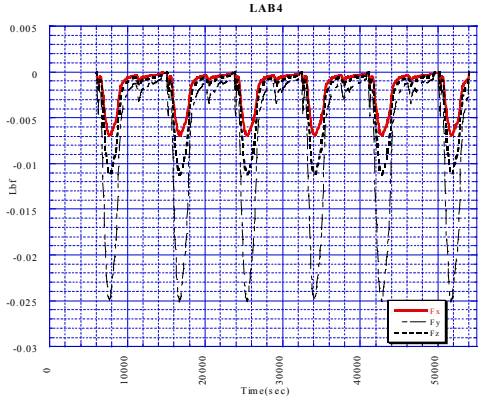
Location	Rack Position in ISS Frame			μG Vector		Unit Vector				Cone Angle	
	X (ft)	Y (ft)	Z (ft)	Magnitude (μG)	⊥ Component (μG)	X	Y	Z	Max angle from unit vector (deg)	⊥ Component @ max angle (μG)	Magnitude at max angle (μG)
CG	-15.34	-1.28	14.87	0.210	0.038	-0.994	-0.107	0.013	20.660	0.025	0.065
USL-C1	15.55	0.00	11.26	0.245	0.064	-0.624	-0.773	-0.119	24.100	0.054	0.122
USL-C2	12.05	0.00	11.26	0.232	0.063	-0.665	-0.722	0.191	26.258	0.050	0.101
USL-C3	8.55	0.00	11.26	0.230	0.070	-0.635	-0.584	0.506	26.070	0.051	0.104
USL-C4	5.05	0.00	11.26	0.243	0.078	-0.546	-0.406	0.733	23.624	0.056	0.129
USL-C5	1.55	0.00	11.26	0.266	0.084	-0.446	-0.247	0.860	20.229	0.062	0.168
USL-S1	15.55	4.84	16.11	0.689	0.087	-0.321	0.068	-0.945	7.346	0.087	0.672
USL-S2	12.05	4.84	16.11	0.645	0.086	-0.340	0.108	-0.934	7.765	0.086	0.628
USL-S3	8.55	4.84	16.11	0.602	0.084	-0.362	0.154	-0.919	8.219	0.084	0.584
USL-S4	5.05	4.84	16.11	0.560	0.083	-0.386	0.207	-0.899	8.793	0.076	0.488
USL-P1	15.55	-4.84	16.11	0.722	0.088	-0.217	-0.488	-0.845	7.082	0.088	0.707
USL-P2	12.05	-4.84	16.11	0.671	0.087	-0.230	-0.497	-0.837	7.551	0.087	0.656
USL-P4	5.00	-4.84	16.11	0.570	0.085	-0.264	-0.519	-0.813	8.725	0.084	0.546
JPM1-A1	29.66	-10.82	15.92	1.035	0.091	-0.126	-0.652	-0.748	5.190	0.091	1.006
JPM2-F1	40.00	-10.82	15.92	1.193	0.093	-0.118	-0.617	-0.778	4.618	0.093	1.156
JPM3-A2	29.66	-14.32	15.92	1.121	0.092	-0.097	-0.726	-0.680	4.810	0.092	1.089
JPM4-F2	40.00	-14.32	15.92	1.274	0.094	-0.094	-0.688	-0.720	4.339	0.094	1.234
JPM5-A3	29.66	-17.82	15.92	1.217	0.092	-0.072	-0.783	-0.617	4.450	0.092	1.182
JPM6-F3	40.00	-17.82	15.92	1.364	0.094	-0.072	-0.744	-0.664	4.068	0.094	1.321
JPM7-A4	29.66	-21.32	15.92	1.320	0.093	-0.050	-0.827	-0.561	4.122	0.093	1.283
JPM8-A5	29.66	-24.82	15.92	1.429	0.093	-0.032	-0.860	-0.510	3.831	0.093	1.392
JPM9-F5	40.00	-24.82	15.92	1.566	0.095	-0.036	-0.825	-0.564	3.585	0.095	1.520
JPM10-F6	40.00	-28.32	15.92	1.675	0.096	-0.021	-0.854	-0.521	3.384	0.096	1.627
APM-CLG1	34.84	14.39	10.74	0.517	0.089	-0.435	0.684	-0.586	9.998	0.089	0.505
APM-CLG2	34.84	18.33	10.74	0.640	0.093	-0.379	0.794	-0.475	8.422	0.093	0.629
APM-FWD1	40.00	14.39	15.91	1.078	0.094	-0.272	0.266	-0.925	5.027	0.094	1.067
APM-FWD2	40.00	18.33	15.91	1.146	0.095	-0.277	0.390	-0.878	4.781	0.095	1.135
APM-FWD3	40.00	22.26	15.91	1.229	0.096	-0.277	0.493	-0.825	4.521	0.096	1.219
APM-FWD4	40.00	26.19	15.91	1.326	0.098	-0.274	0.576	-0.771	4.267	0.098	1.316
APM-AFT1	29.67	14.39	15.91	0.963	0.092	-0.297	0.366	-0.882	5.528	0.092	0.951
APM-AFT2	29.67	18.33	15.91	1.045	0.094	-0.295	0.491	-0.820	5.173	0.094	1.033
APM-AFT3	29.67	22.26	15.91	1.142	0.095	-0.290	0.587	-0.756	4.824	0.095	1.131
APM-AFT4	29.67	26.19	15.91	1.251	0.098	-0.282	0.661	-0.695	4.504	0.098	1.242
CAM-MID	36.08	0.00	4.17	0.608	0.091	-0.045	-0.410	0.911	8.877	0.091	0.581
CAM-TOP	36.08	0.00	0.00	1.077	0.092	0.033	-0.216	0.976	5.019	0.092	1.042

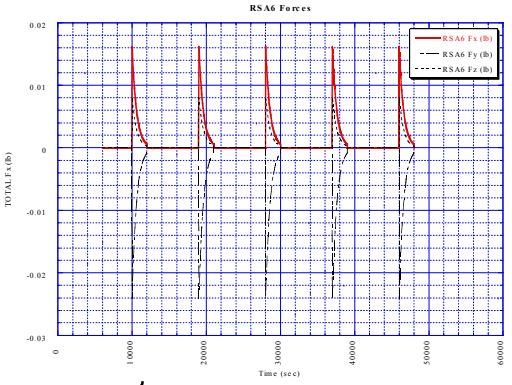
DAC8 Quasi-steady Individual Disturbance Inputs

- **Centrifuge startup and shut down**
  - **Spin-up for 120 sec to 236 deg/s, spin for 6.4 hours, spin-down for 120 sec.**
  - **Starts at 17000 sec**
- **TRRJ slew at low betas**
  - **TRRJ 0 beta slew rates - TRRJ Torque Power Spectral Density has 87.7% of its power below .01 Hz.**
  - **Not Applicable**
- **Solar Thermal base loads**
  - **Exponential decay for 210 seconds every 2160 seconds (night), 3360 (day), forces combined for eight arrays**
  - **Lighting dependent , continuous**
- **LAB4 Vent**
  - **Force profile, duration of 8700 seconds**
  - **Starts at 6000 seconds**
- **RSA6 Vent**
  - **Exponential decay of 600 seconds every 9000 seconds**
  - **Starts at 10000 seconds**
- **Treadmill Gyro Start-up**
  - **+.23 ft-lbs. for 10minutes, 0 ft-lbs. for 60 minutes, -.23 ft-lbs. for 10 minutes, repeated every 30 minutes.**
  - **Starts at 6000 seconds**

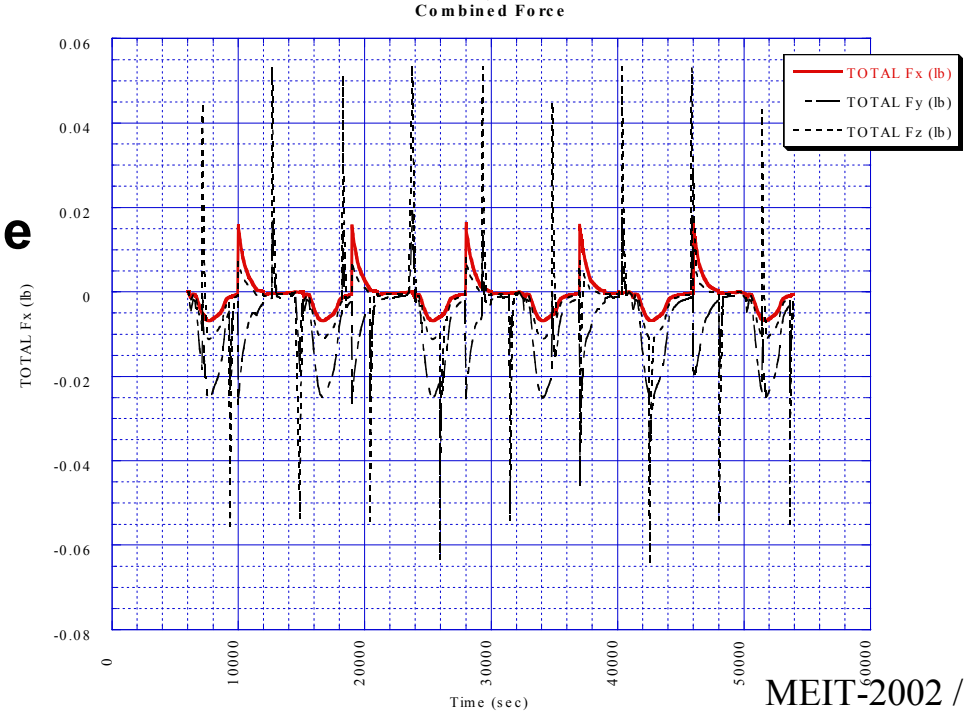
DAC8 Quasi-steady Individual Disturbance Inputs



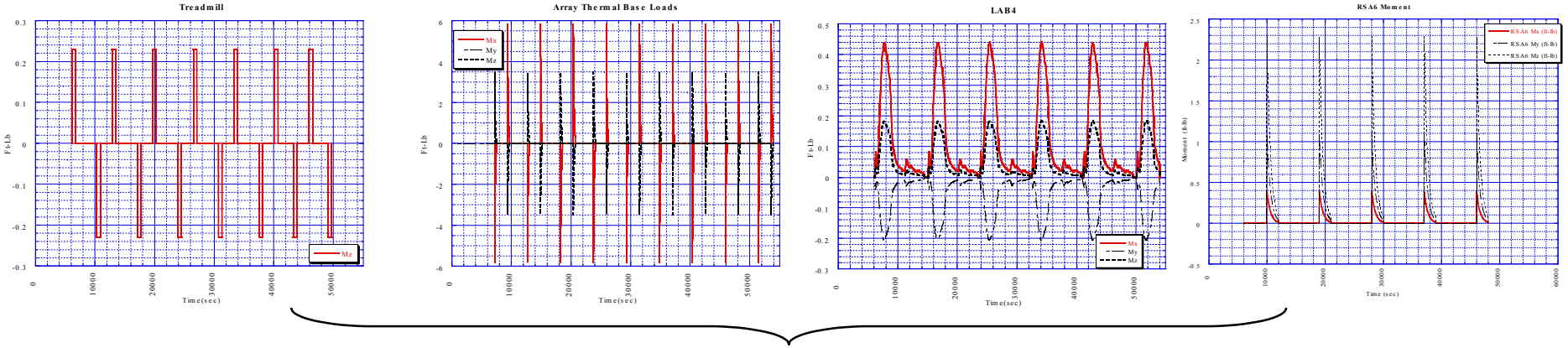




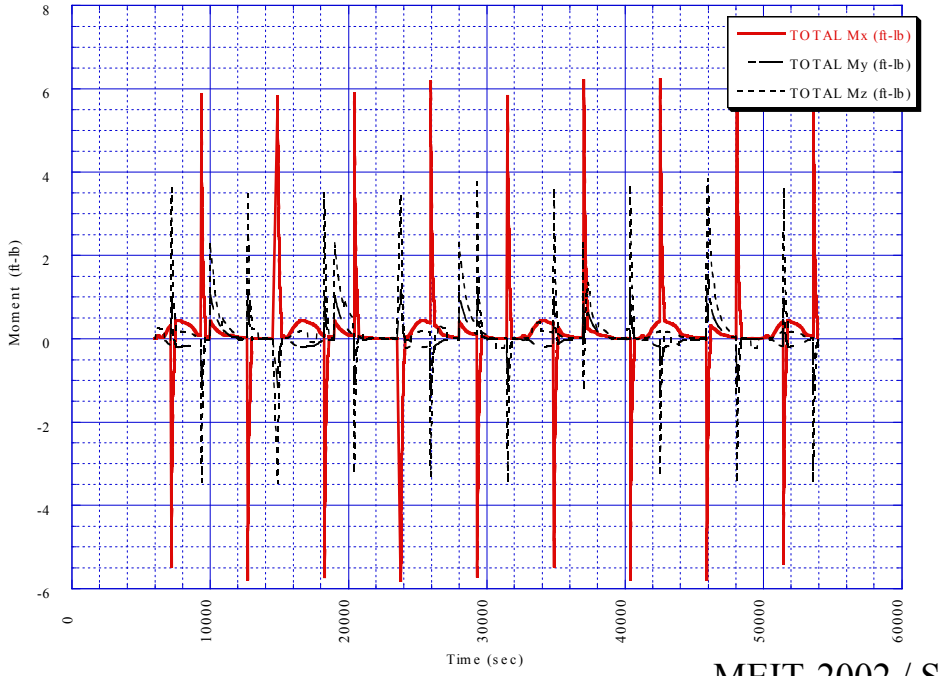
Force files combined into one file



DAC8 Quasi-steady Individual Disturbance Inputs



COMBINED MOMENTS



Moments combined into one file

DAC8 Quasi-Steady Performance With Individual Disturbances Delta Comparison

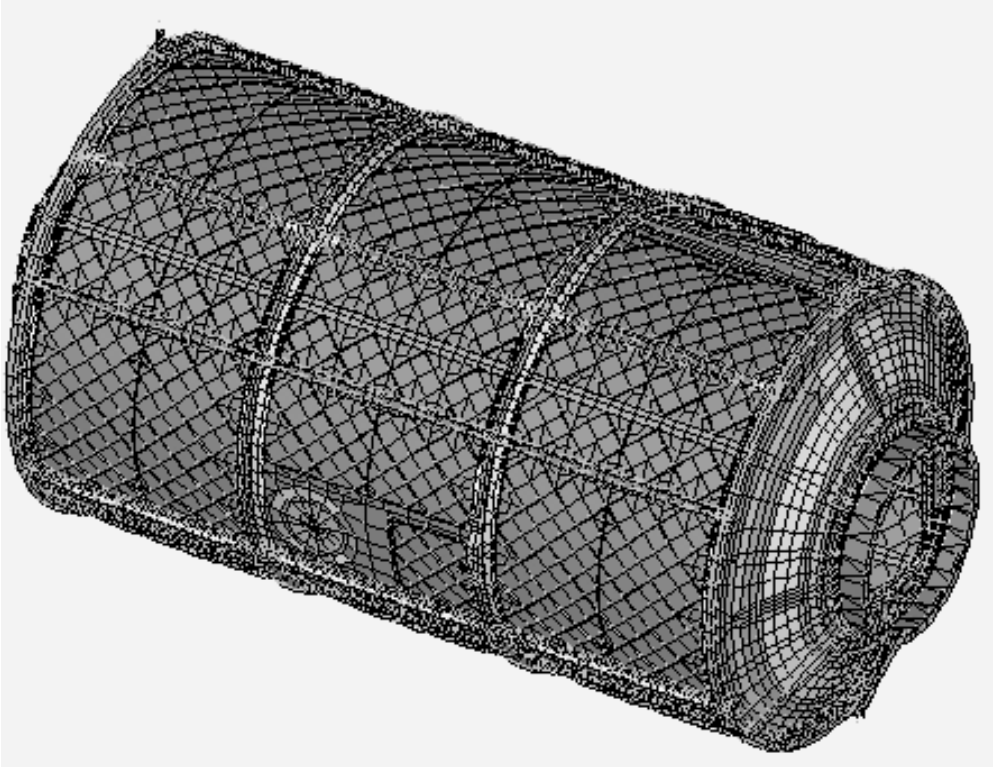
14 versus 15 of 32 racks under 1 μg magnitude and .2 μg perpendicular component (APM AFT1 to 1.068 & 0.22)

Location	Magnitude Disturbance (μG)	Magnitude Nominal (μG)	Magnitude Delta Dist-Nom (μG)	Mag % Difference	⊥ Component Disturbance (μG)	⊥ Component Nominal (μG)	⊥ Component Delta Dist-Nom (μG)	⊥ Component % Difference
CG	0.211	0.210	0.001	0%	0.080	0.046	0.203	74%
USL-C1	0.293	0.245	0.048	20%	0.158	0.064	0.094	147%
USL-C2	0.269	0.232	0.037	16%	0.150	0.063	0.087	138%
USL-C3	0.258	0.230	0.028	12%	0.140	0.070	0.070	100%
USL-C4	0.259	0.243	0.016	7%	0.128	0.078	0.050	64%
USL-C5	0.293	0.266	0.027	10%	0.116	0.084	0.032	38%
USL-S1	0.711	0.689	0.022	3%	0.170	0.087	0.083	95%
USL-S2	0.668	0.645	0.023	4%	0.156	0.086	0.070	81%
USL-S3	0.625	0.602	0.023	4%	0.142	0.084	0.058	69%
USL-S4	0.584	0.560	0.024	4%	0.128	0.083	0.045	54%
USL-P1	0.791	0.722	0.069	10%	0.139	0.088	0.051	58%
USL-P2	0.735	0.671	0.064	10%	0.127	0.087	0.040	46%
USL-P4	0.623	0.570	0.053	9%	0.105	0.085	0.020	24%
JPM1-A1	1.132	1.035	0.097	9%	0.150	0.091	0.059	65%
JPM2-F1	1.293	1.193	0.100	8%	0.188	0.093	0.095	102%
JPM3-A2	1.225	1.121	0.104	9%	0.153	0.092	0.061	66%
JPM4-F2	1.383	1.274	0.109	9%	0.172	0.094	0.078	83%
JPM5-A3	1.327	1.217	0.110	9%	0.157	0.092	0.065	71%
JPM6-F3	1.480	1.364	0.116	9%	0.174	0.094	0.080	85%
JPM7-A4	1.435	1.320	0.115	9%	0.162	0.093	0.069	74%
JPM8-A5	1.547	1.429	0.118	8%	0.168	0.093	0.075	81%
JPM9-F5	1.691	1.566	0.125	8%	0.183	0.095	0.088	93%
JPM10-F6	1.804	1.675	0.129	8%	0.189	0.096	0.093	97%
APM-CLG1	0.710	0.517	0.193	37%	0.151	0.089	0.062	70%
APM-CLG2	0.856	0.640	0.216	34%	0.133	0.093	0.040	43%
APM-FWD1	1.184	1.078	0.106	10%	0.268	0.094	0.174	185%
APM-FWD2	1.283	1.146	0.137	12%	0.259	0.095	0.164	173%
APM-FWD3	1.393	1.229	0.164	13%	0.249	0.096	0.153	159%
APM-FWD4	1.513	1.326	0.187	14%	0.242	0.098	0.144	147%
APM-AFT1	1.068	0.963	0.105	11%	0.219	0.092	0.127	138%
APM-AFT2	1.176	1.045	0.131	13%	0.211	0.094	0.117	124%
APM-AFT3	1.296	1.142	0.154	13%	0.206	0.095	0.111	117%
APM-AFT4	1.423	1.251	0.172	14%	0.206	0.098	0.108	110%
CAM-MID	0.650	0.608	0.042	7%	0.238	0.091	0.147	162%
CAM-TOP	1.100	1.077	0.023	2%	0.252	0.092	0.160	174%

US Lab Model Frequencies

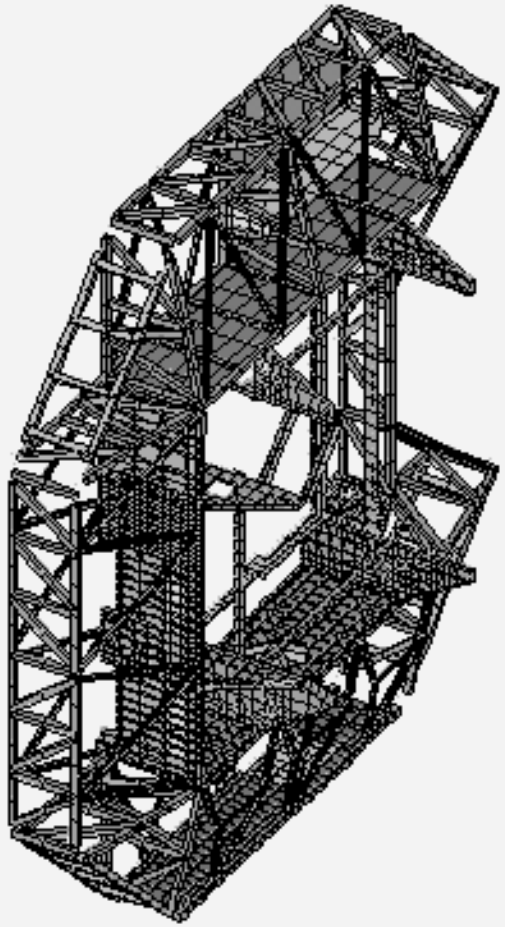
9.29E-04	Rigid Body Mode
1.60E-03	Rigid Body Mode
2.06E-03	Rigid Body Mode
2.33E-03	Rigid Body Mode
2.69E-03	Rigid Body Mode
3.93E-03	Rigid Body Mode
2.39E+00	
2.83E+00	
2.89E+00	
2.99E+00	
3.04E+00	
3.08E+00	
3.12E+00	
3.29E+00	
3.39E+00	
3.62E+00	
3.75E+00	
4.04E+00	

Integrated US Lab Model

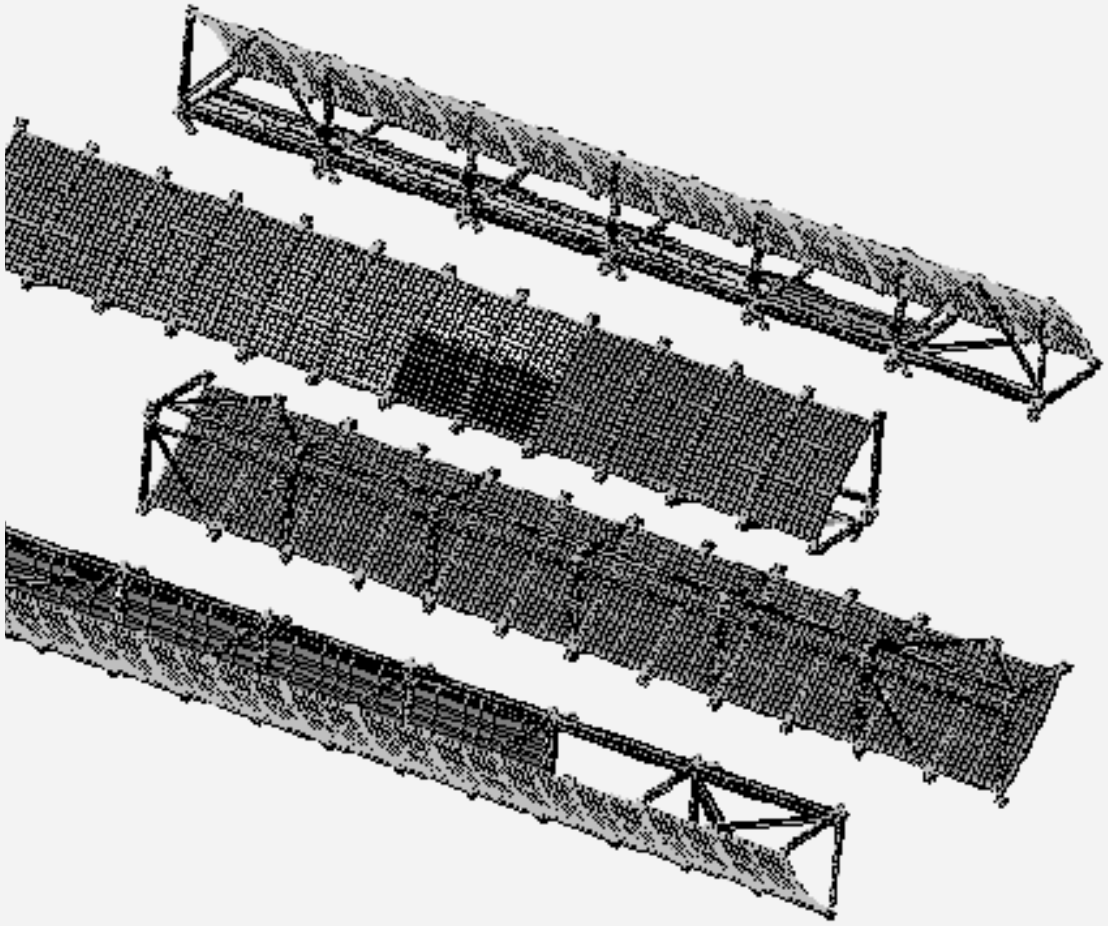


DAC8 Finite Element Model

Aft ESS

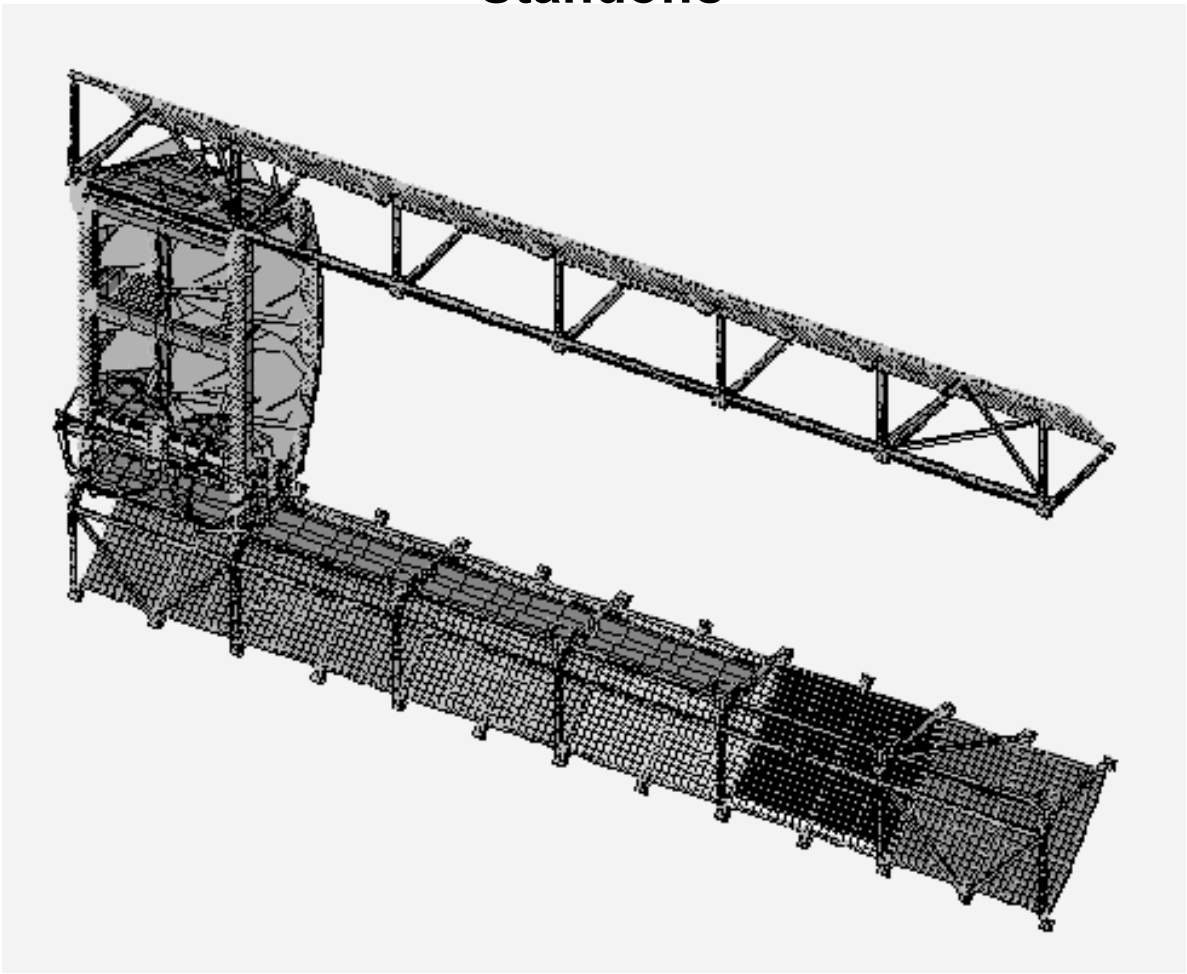


Standoffs



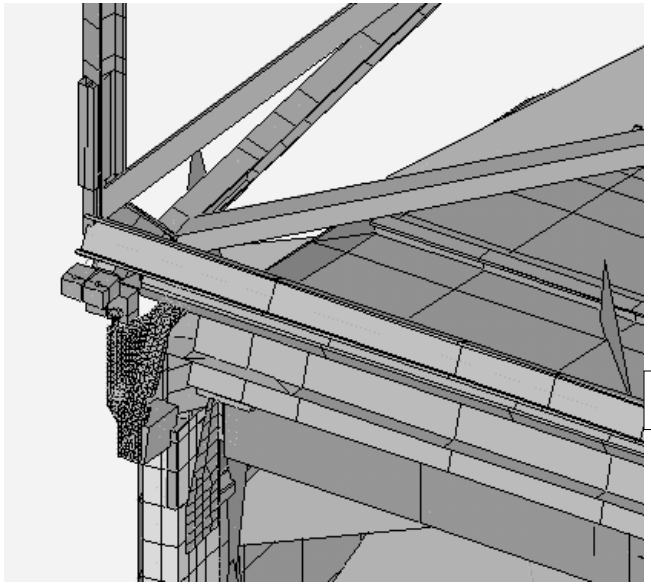
DAC8 Finite Element Model

Rack Integrated with Standoffs

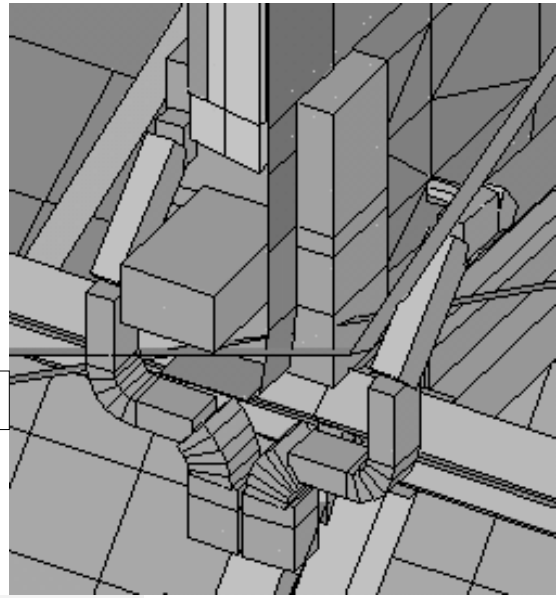


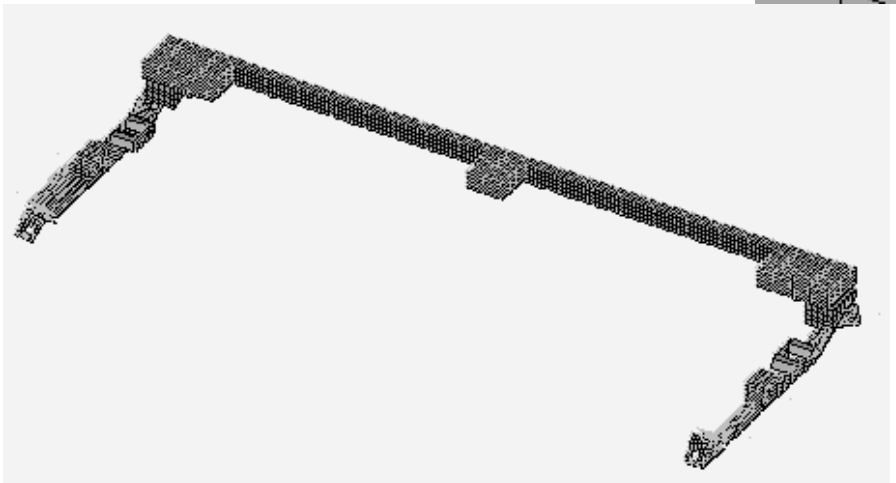
DAC8 Finite Element Model

K-Bar



Pivot Pins

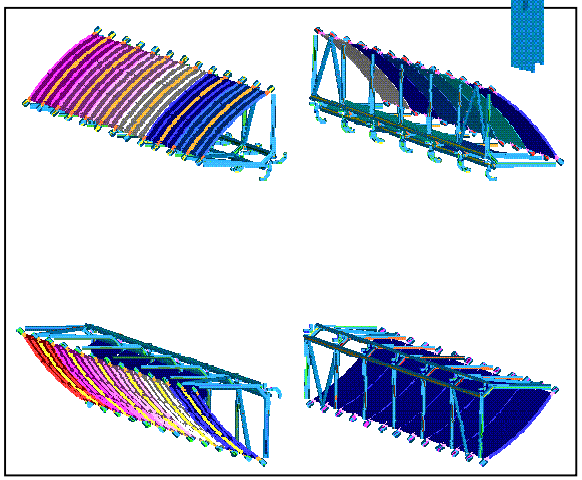




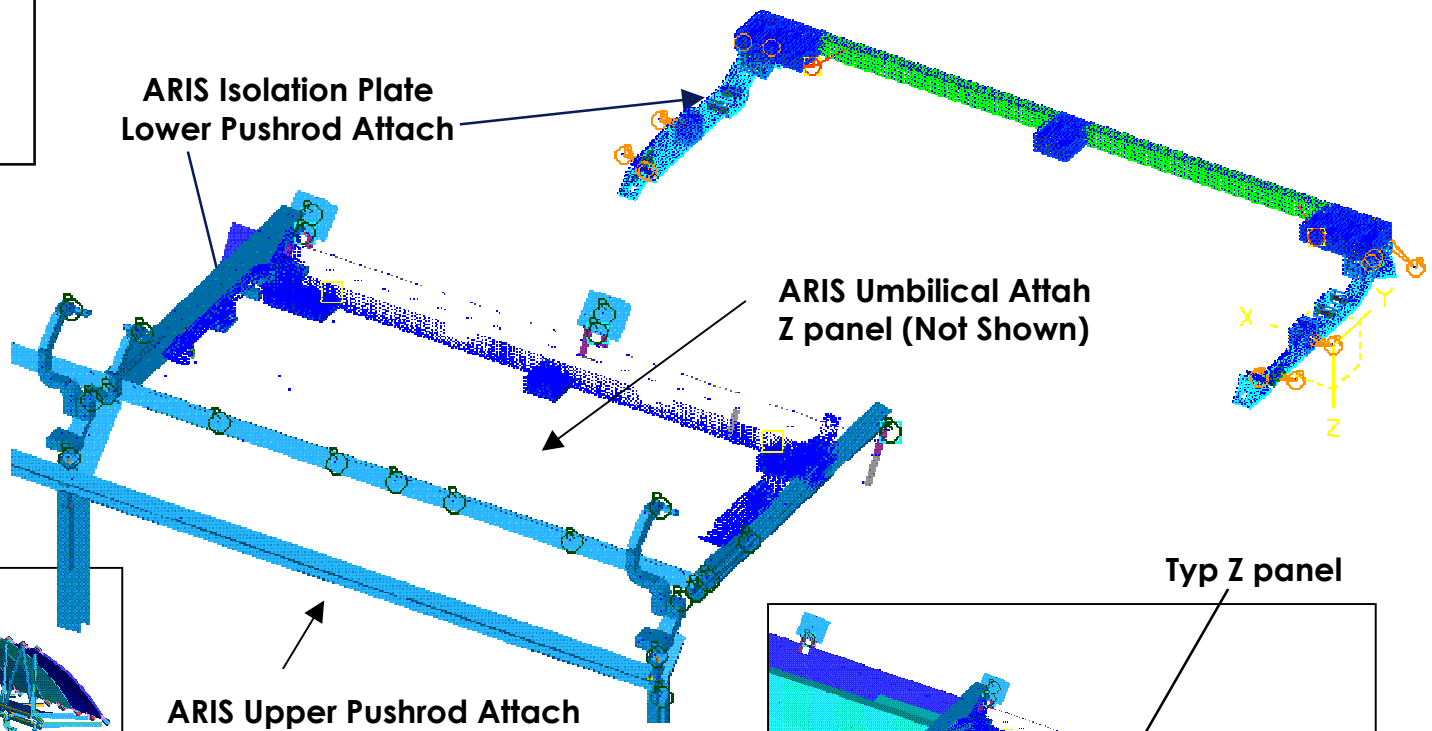
Isolation Plate

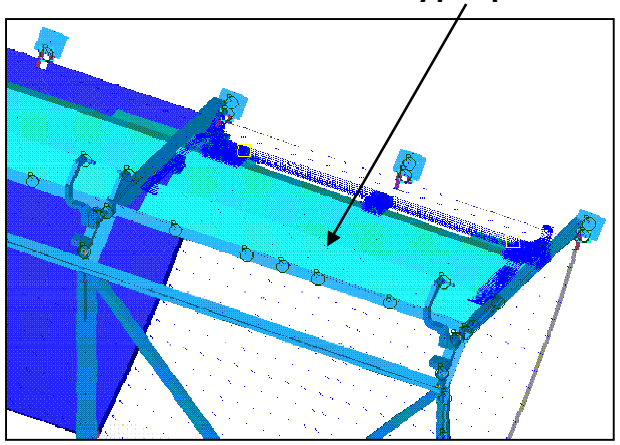
Requirement Applicability

@ 50% Of ISPRs In APM/JEM/LAB Vibratory @ Rack To Module Interface

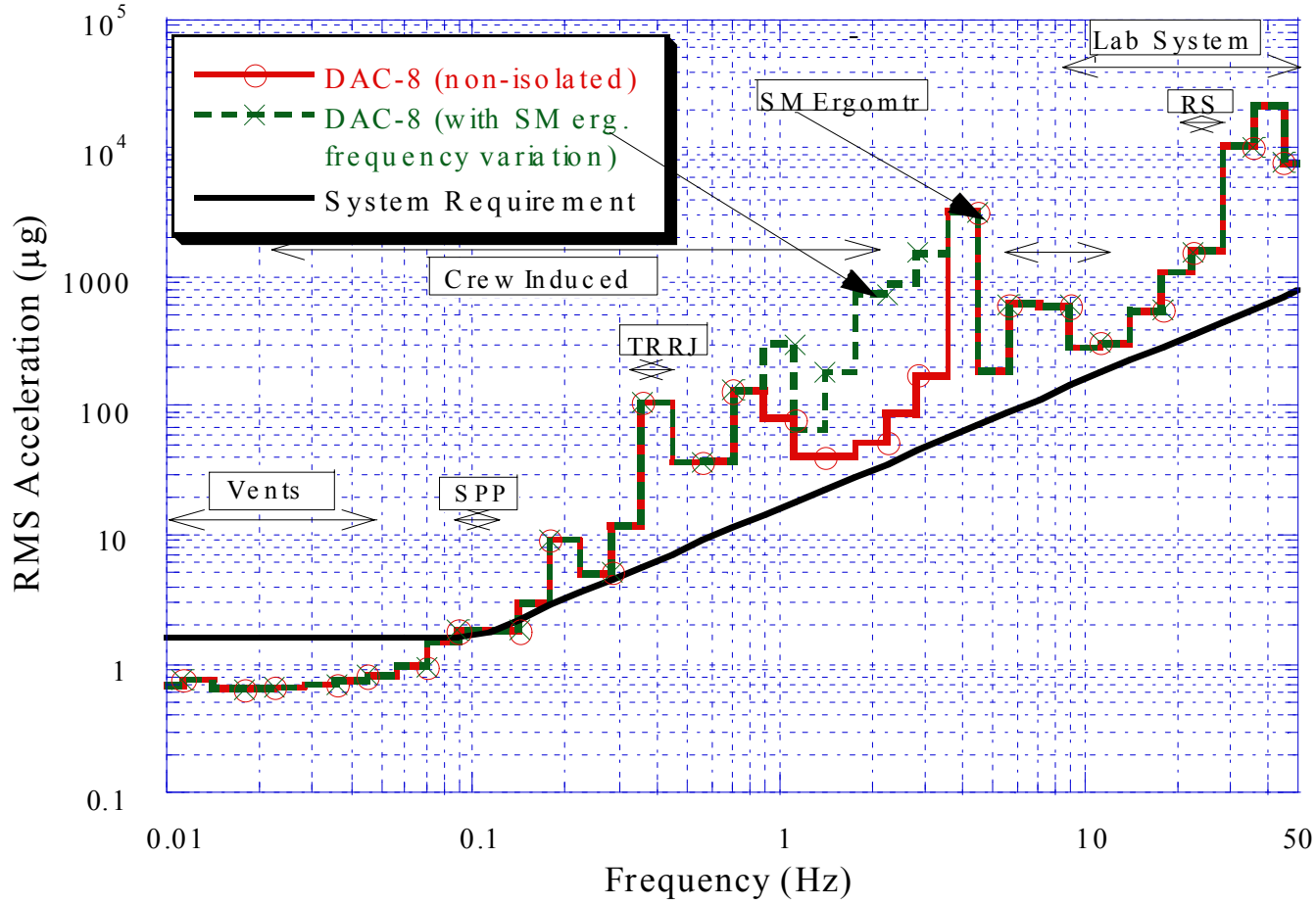


Lab Standoffs

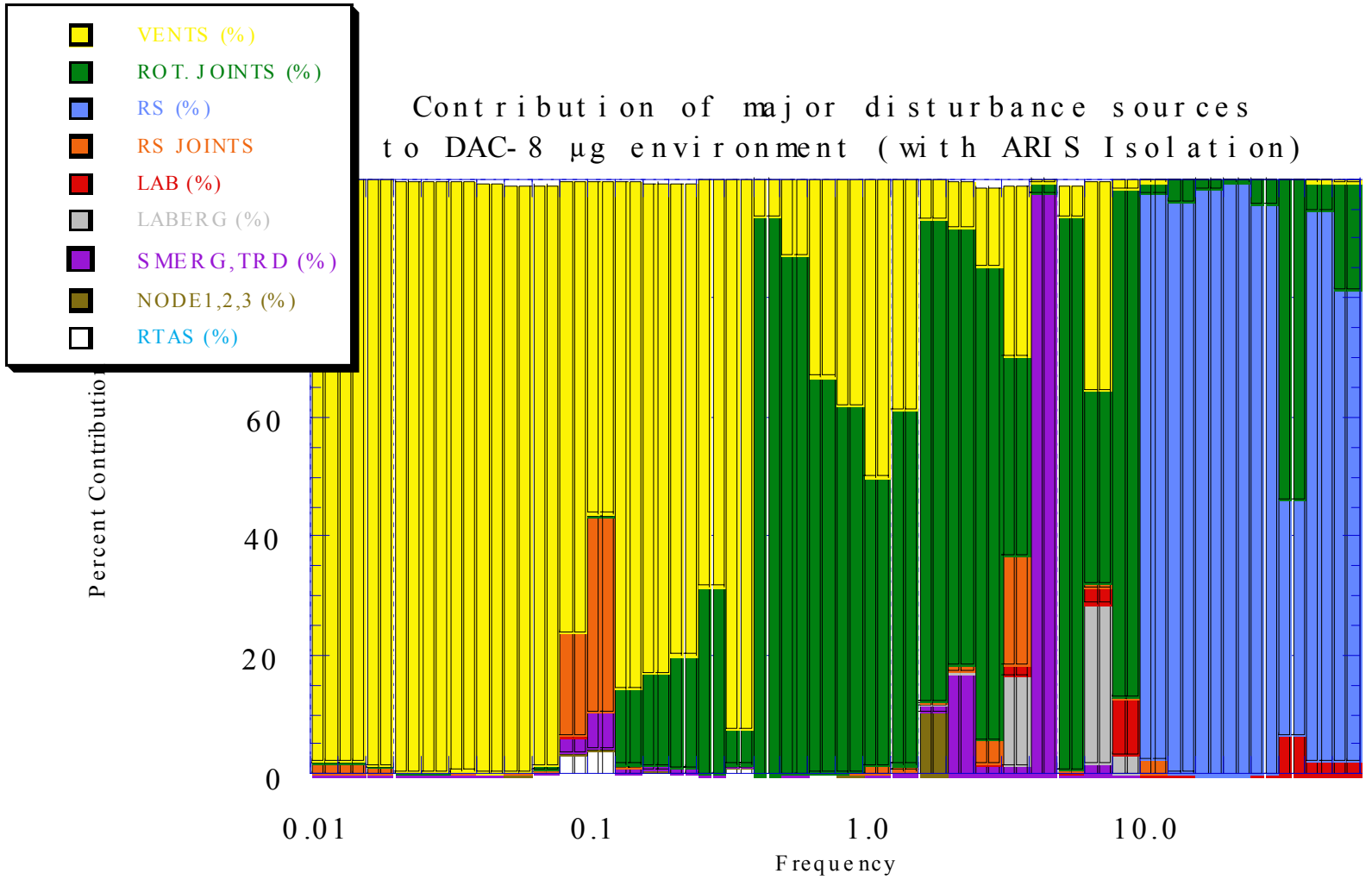




DAC8 Non-Isolated Performance
Structural Dynamic Frequency Range



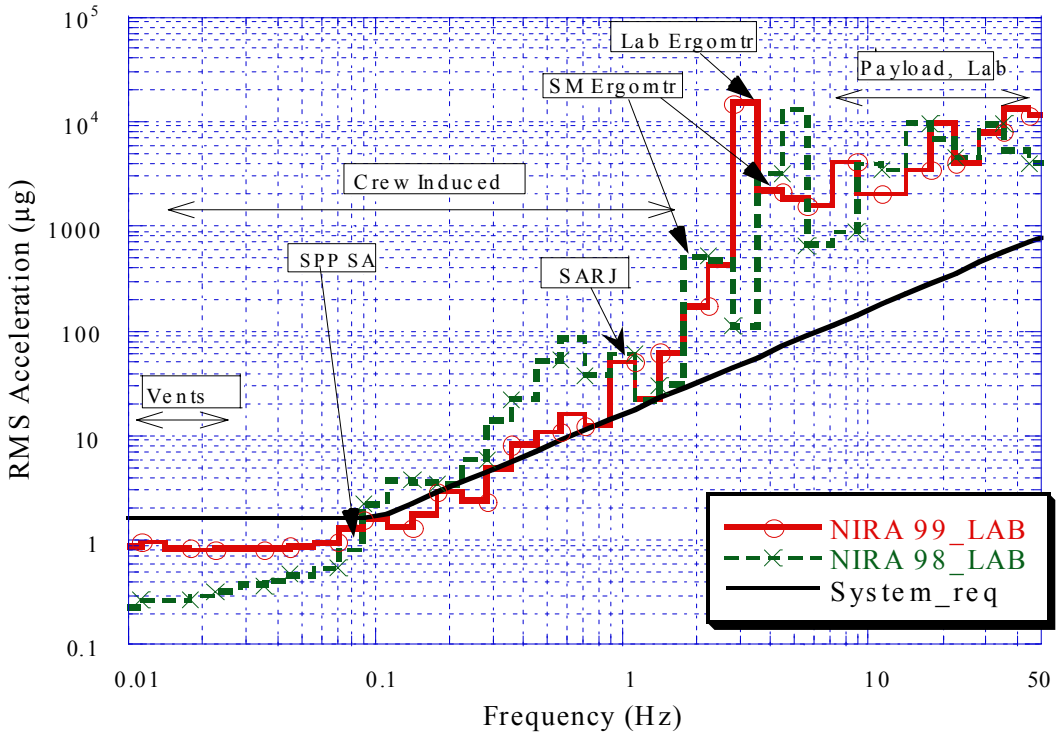
DAC8 Performance
Structural Dynamic Frequency Range



NIRA 99 - US Lab
Structural Dynamic Frequency Range

Non-Isolated Rack Assessment Differences From DAC8 Requirement Compliance Results

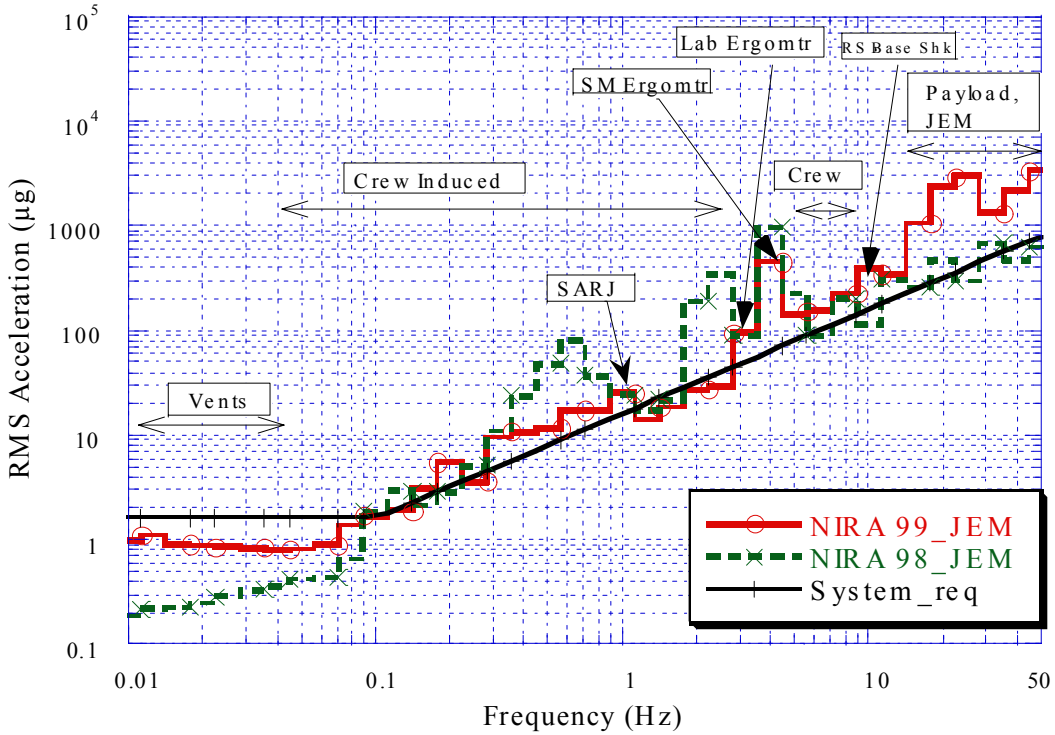
- 1% Damping
- + 2Crew translations & 2console ops
- + Payload disturbances (8 racks in Lab, 3 in COF and 2 in JEM)(21 sources per rack includes AAA fan.)
- @ Non-isolated rack interfaces
- Non-isolated Lab ergometer - subsequently isolated (see DAC8)



NIRA 99 - JEM-PM
Structural Dynamic Frequency Range

Non-Isolated Rack Assessment Differences From DAC8 Requirement Compliance Results

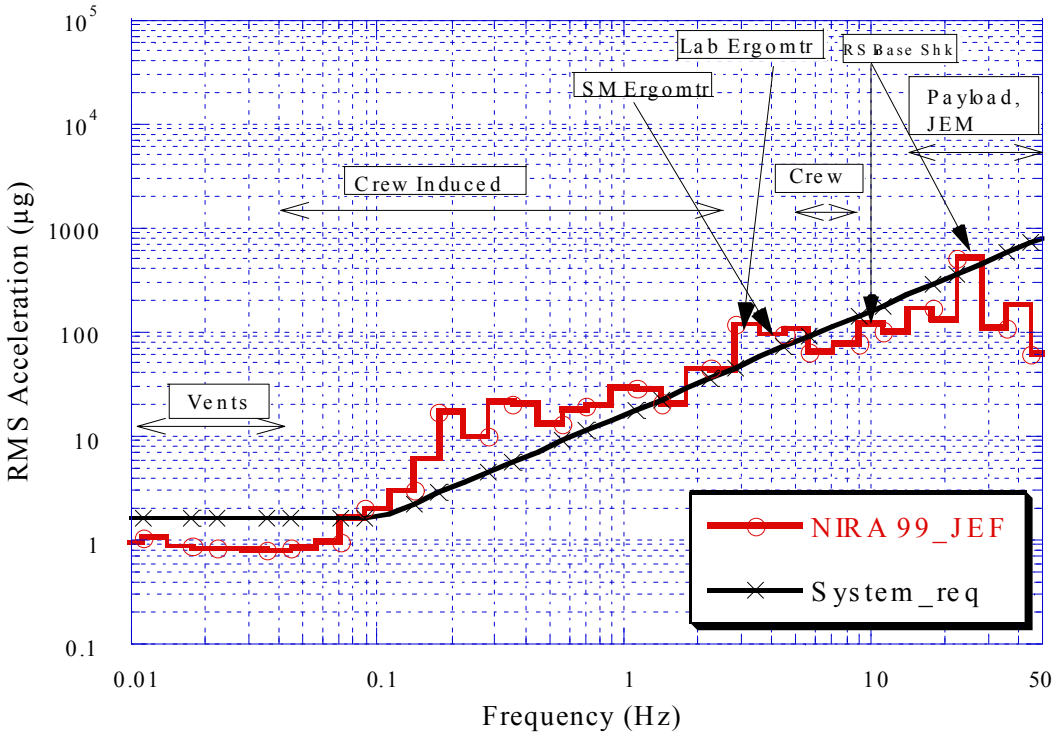
- 1% Damping
- + 2Crew translations & 2console ops
- + Payload disturbances (8 racks in Lab, 3 in COF and 2 in JEM)(21 sources per rack includes AAA fan.)
- @ Non-isolated rack interfaces
- Non-isolated Lab ergometer - subsequently isolated (see DAC8)



NIRA 99 - JEM-EF
Structural Dynamic Frequency Range

Non-Isolated Rack Assessment Differences From DAC8 Requirement Compliance Results

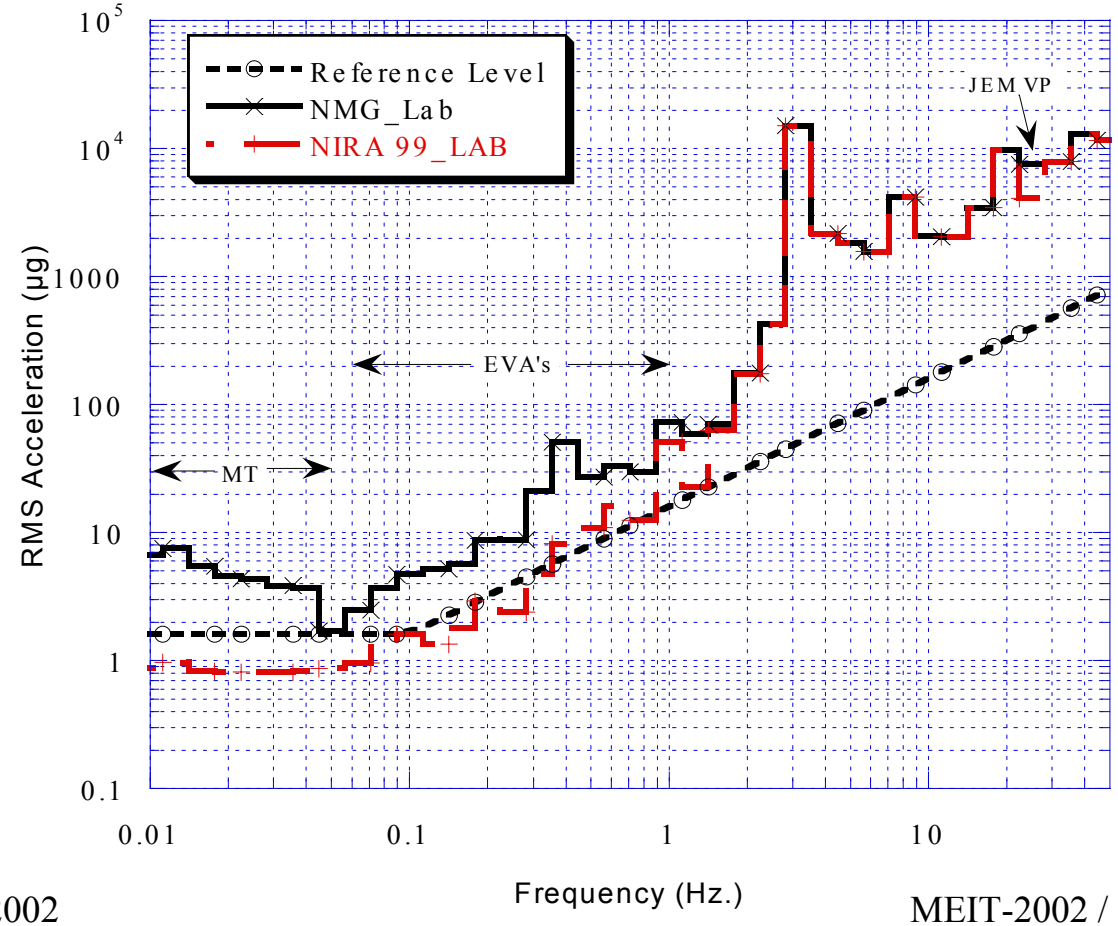
- 1% Damping
- + 2Crew translations & 2console ops
- + Payload disturbances (8 racks in Lab, 3 in COF and 2 in JEM)(21 sources per rack includes AAA fan.)
- @ Non-isolated rack interfaces
- Non-isolated Lab ergometer - subsequently isolated (see DAC8)



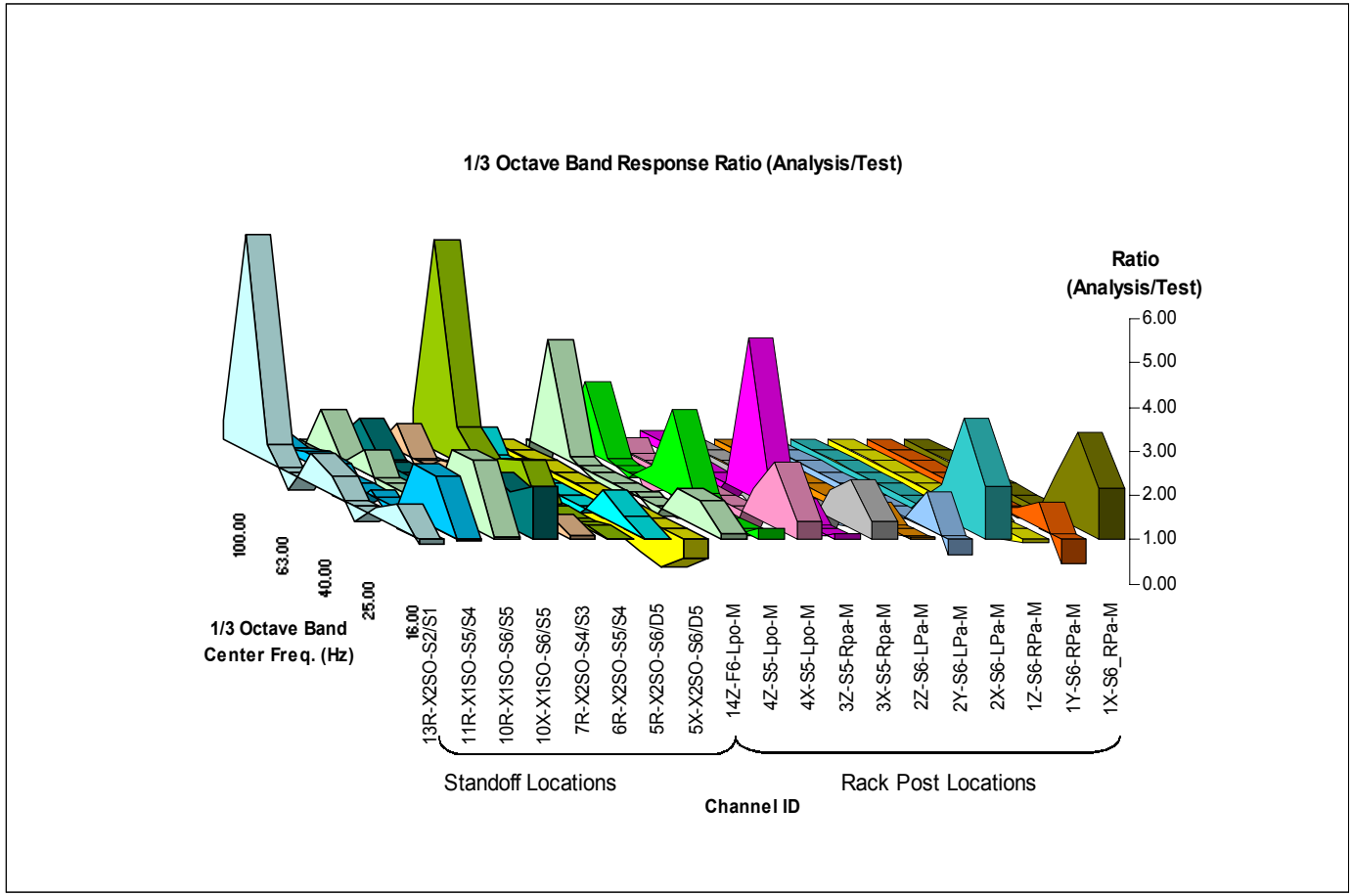
Non-Microgravity Mode (External Ops Case) - U.S. Lab Structural Dynamic Frequency Range

Non-Microgravity Mode Differences From NIRA-99

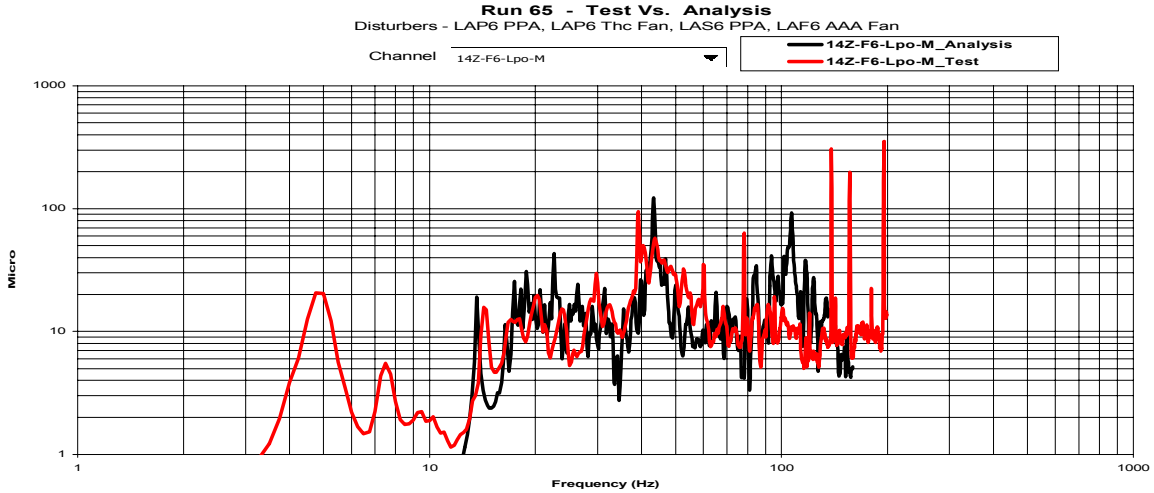
- Add non-microgravity mode disturbances to NIRA-99
- External Operations Case presented includes 2 EVA's, JEM Airlock and Mobile Transporter ops
- Other cases examined focused on thruster activity - reboost, CMG de-saturation, attitude hold
- Cases still to be examined: docking, berthing, rack rotation, et cetera

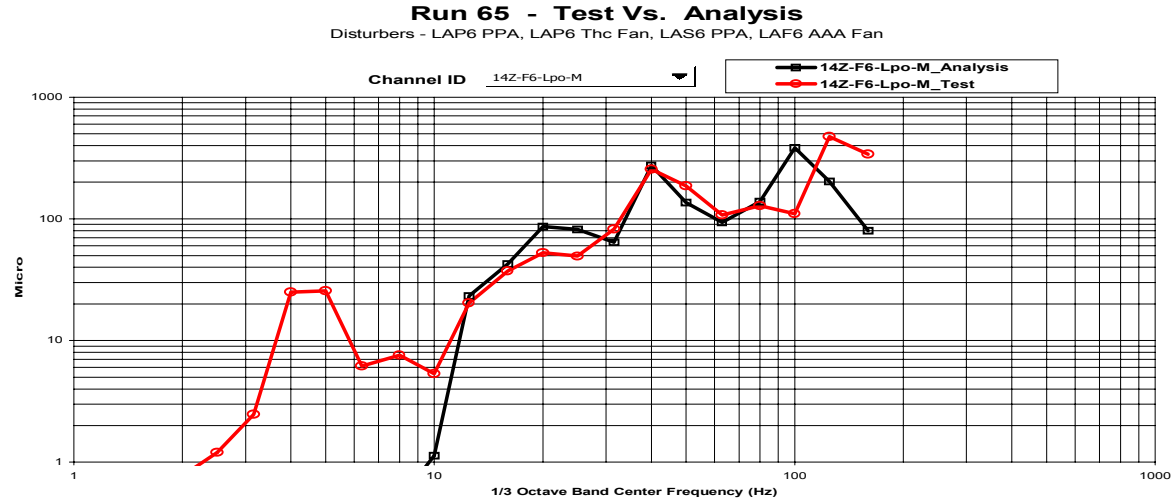


U.S. Lab Ground Test To Analysis Comparison With Ground Test Finite Element Model

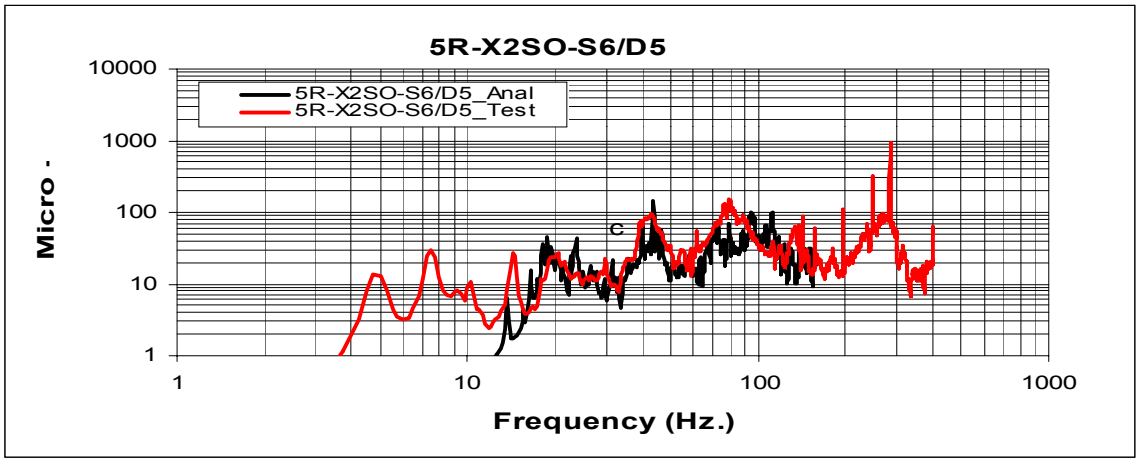


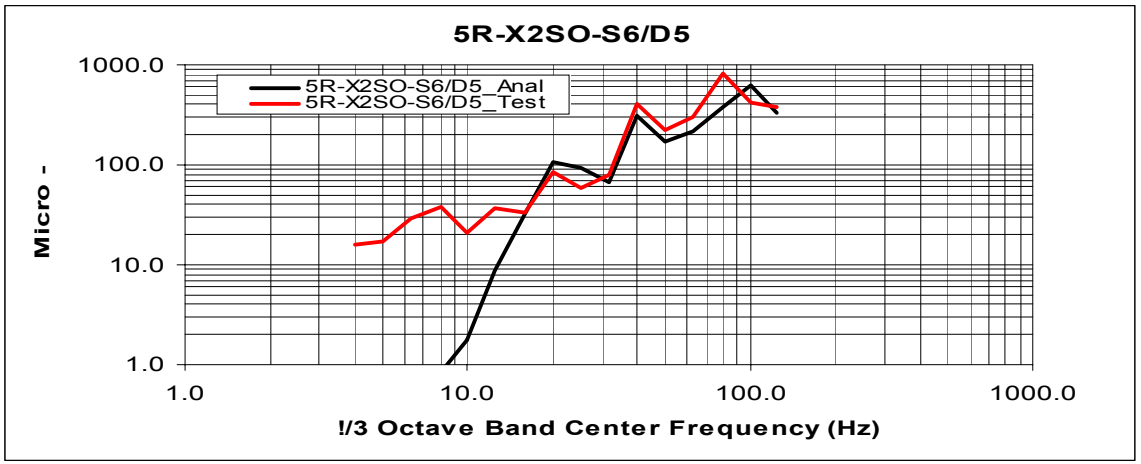
U.S. Lab Ground Test To Analysis Comparison
Rack F6 Response



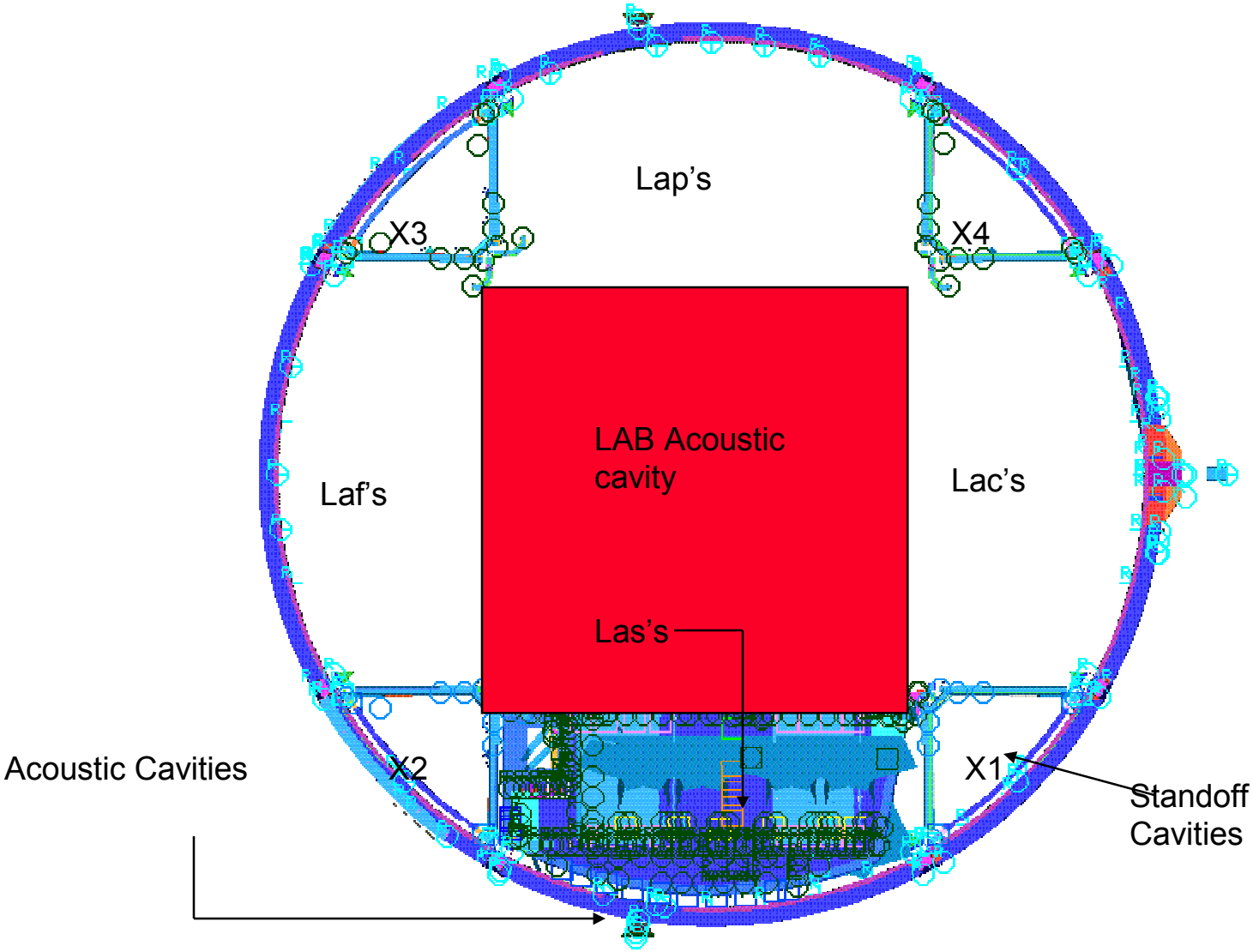


U.S. Lab Ground Test To Analysis Comparison
Standoff S6/S5 Response

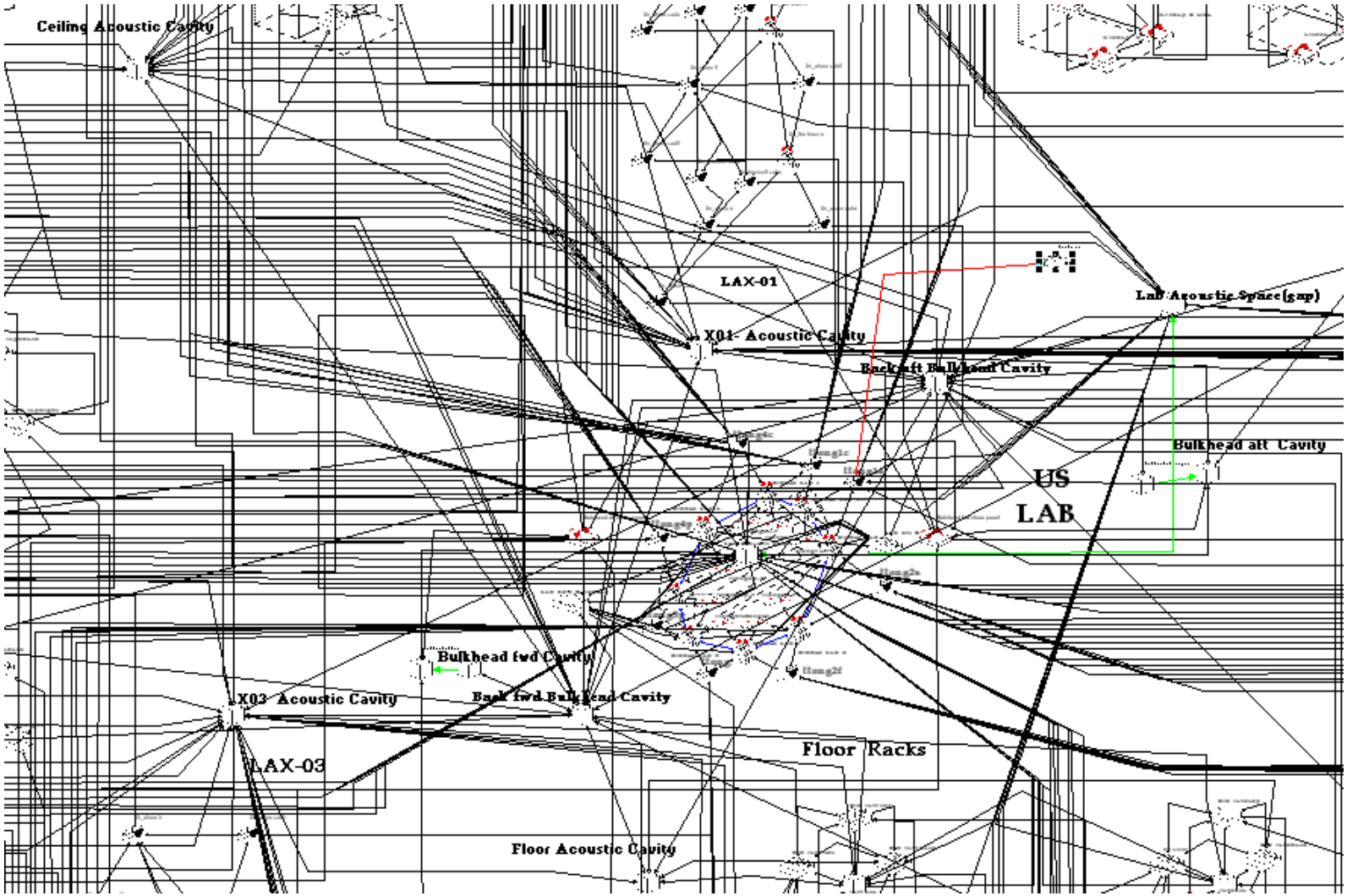




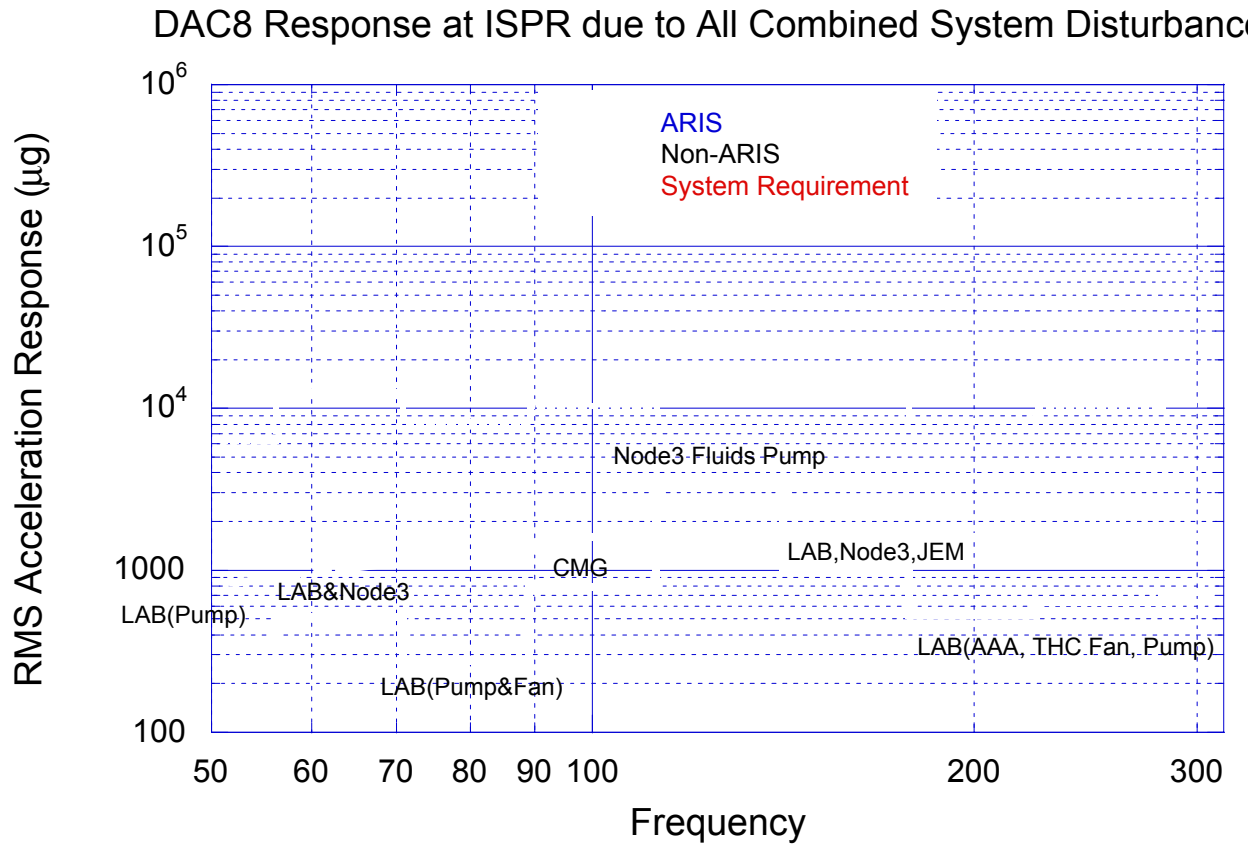
DAC8 Statistical Energy Analysis Model



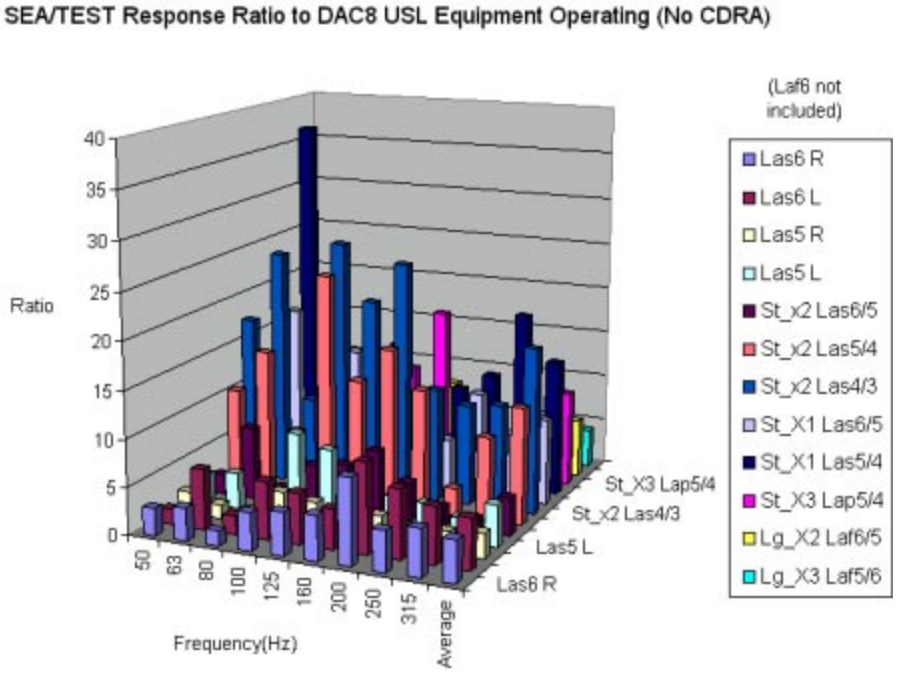
DAC8 Statistical Energy Analysis Model

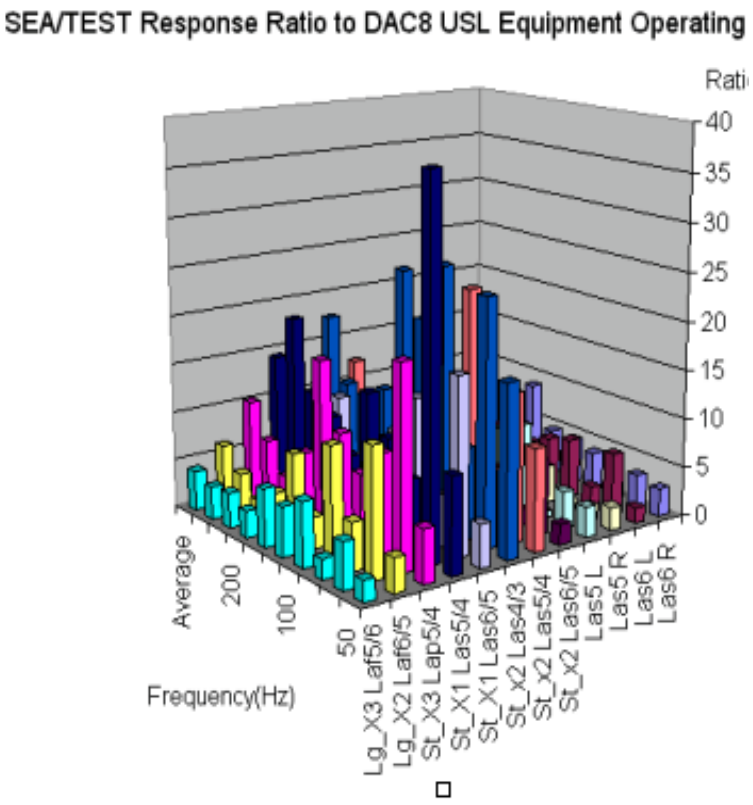


DAC8 Performance
Vibroacoustic Frequency Range



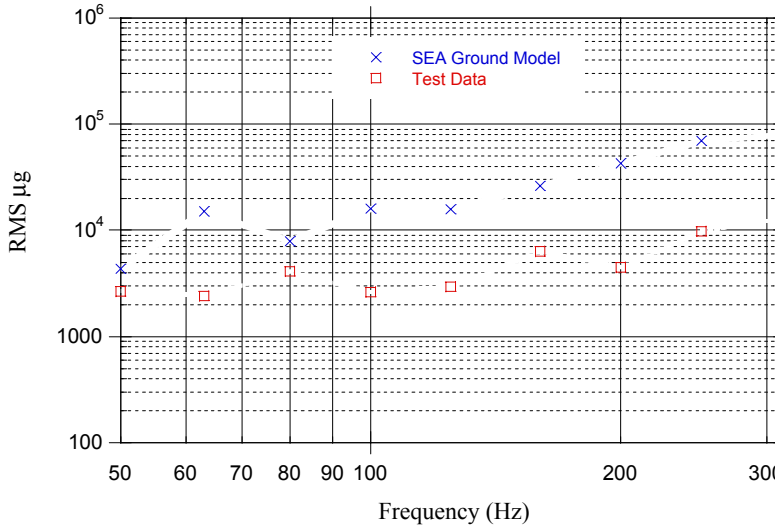
U.S. Lab Ground Test To Analysis Comparison With Ground Test Statistical Energy Model



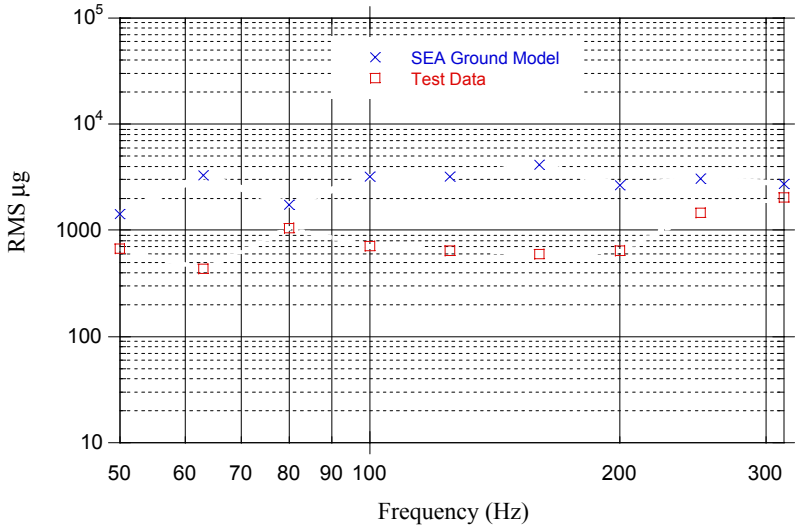


U.S. Lab Ground Test To Analysis Comparison
Rack and Standoff Response

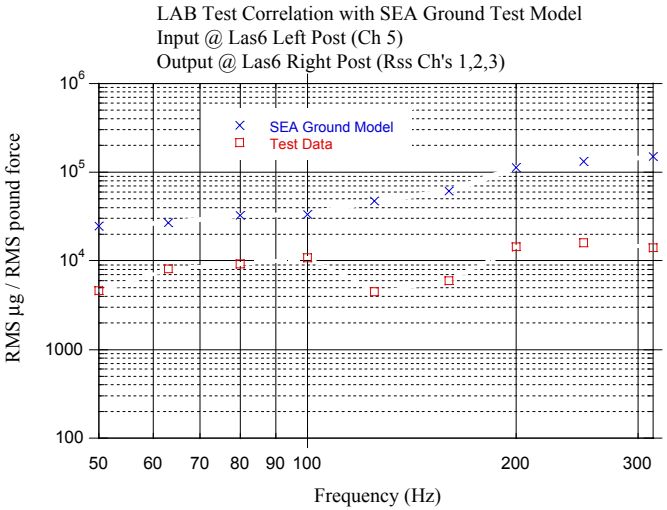
LAB Test Correlation with SEA Ground Test Model
Input @ All USL Equipment Operating (No CDRA)
Output @ Las6 Left Post (Rss Ch's 4,5,6)

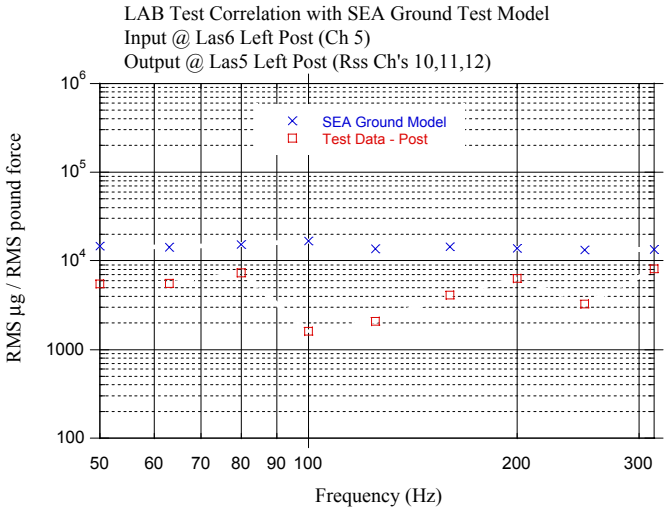


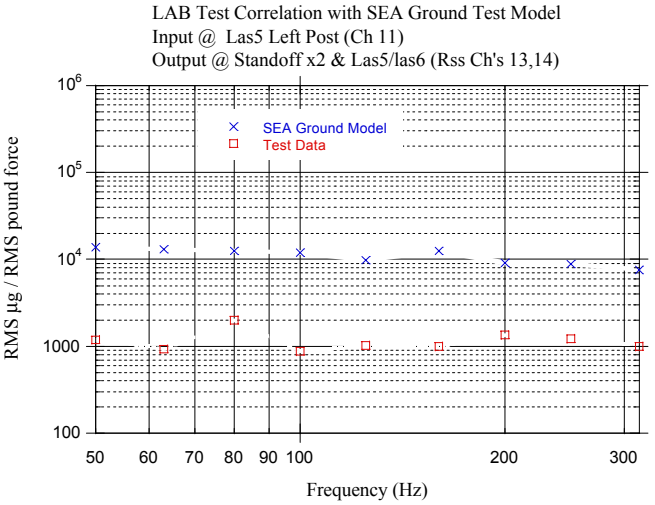
LAB Test Correlation with SEA Ground Test Model
Input @ All USL Equipment Operating (No CDRA)
Output @Standoff X2 Las5/Las6 (Rss Ch's 13,14)

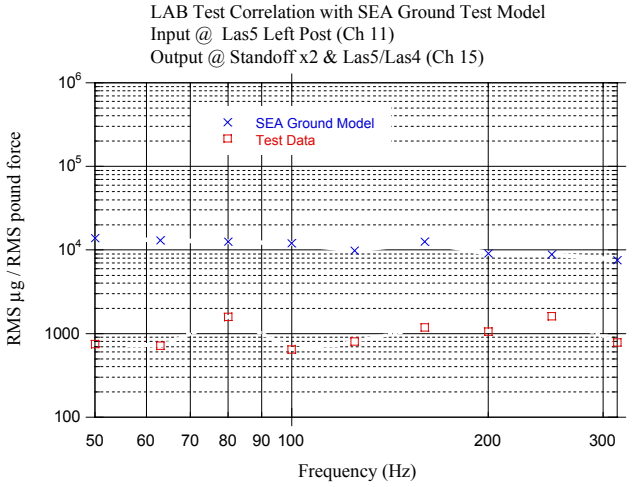


U.S. Lab Ground Test To Analysis Comparison Transfer Functions



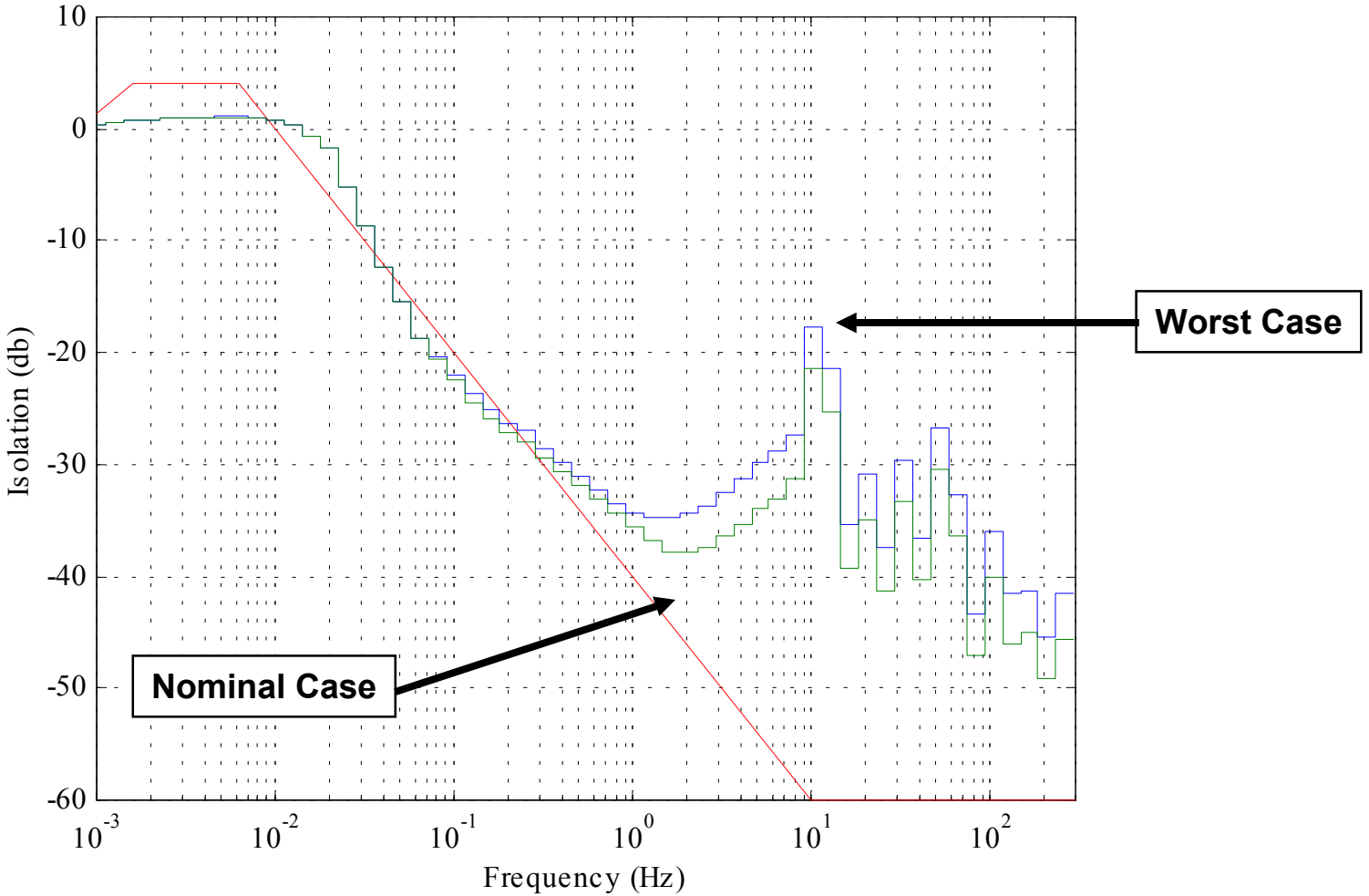




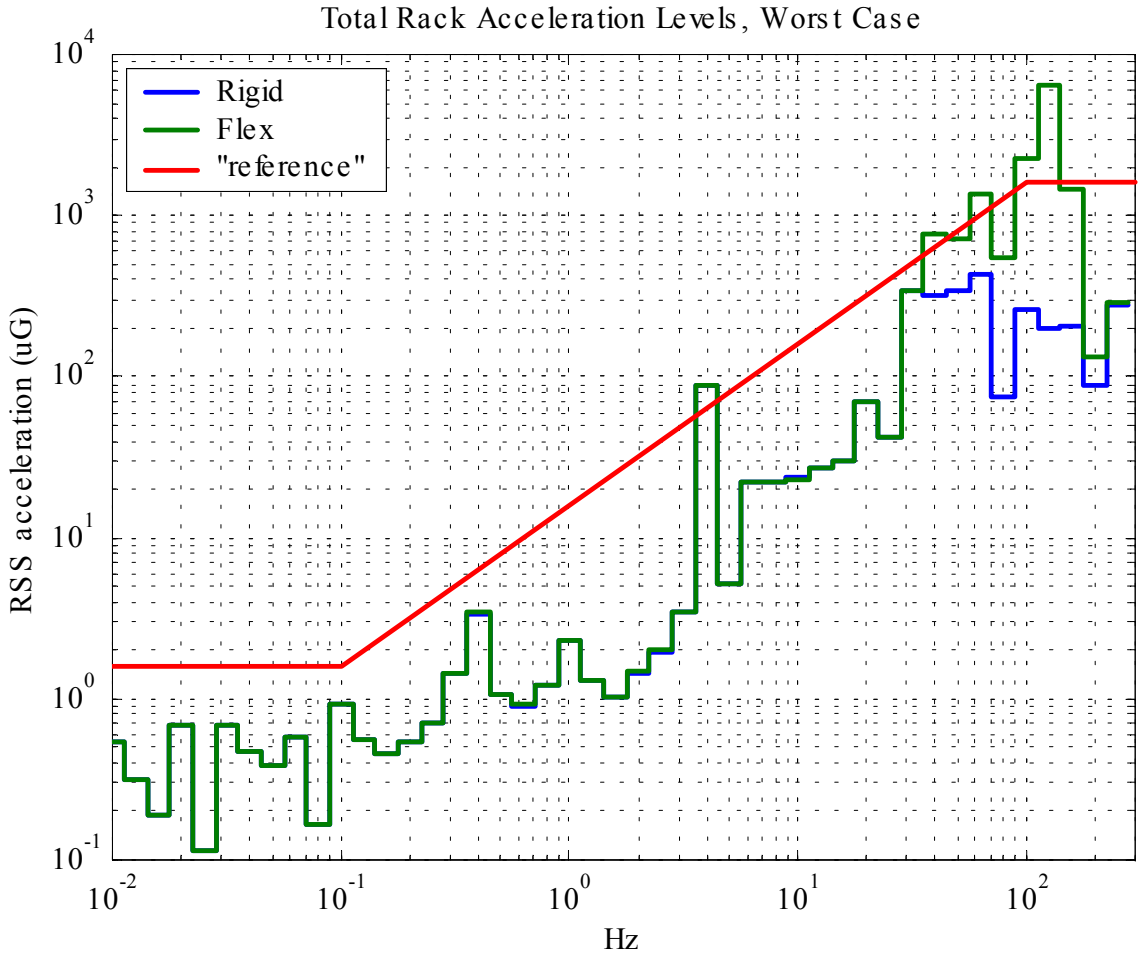


ARIS Isolation Performance

Worst case & Nominal isolation, CG Variations, Worst VP, Worst Input Direction, Worst Ksmall corner 3 or 5, Rigid Rack



Total Isolated Rack Acceleration Levels (ARIS Verification Conditions)



Major updates for DAC-9 Finite Element Model

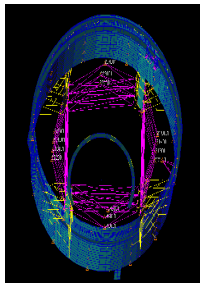
- CONFIGURATION
  - DAC-8 system model represented Rev.C configuration. This was updated to Rev. F configuration for DAC-9, major differences in Russian segment
  - Node 4 / Propulsion module not included.

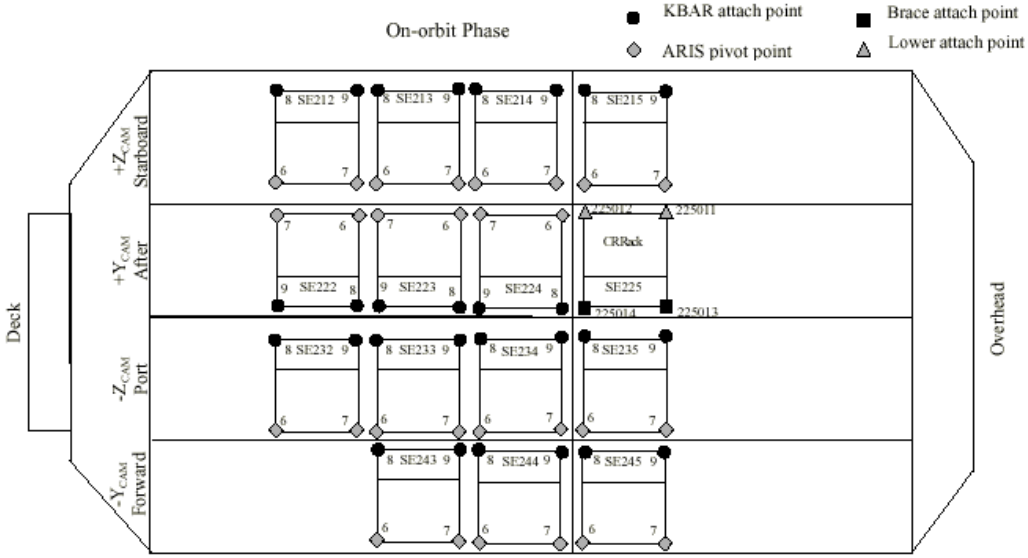
• COMPONENT MODELS	SOURCE
• US Laboratory Module (US Lab) With All System Racks	Boeing Hsv
• Japanese Experiment Module (JEM) With Test Correlated PM & ELM-PS	NASDA
• ESA Attached Pressurized Module (APM) Detailed Update	ESA
• Centrifuge Accommodation Module (CAM) With Rotor Instead of Boeing Generated JEM Derivative Model With Point Rotor	NASDA/ARC
• Node 2 and Node 3 Instead of Node 1 Duplicate	Alenia
• Photo-Voltaic Arrays To 50 Hz Instead of 25 Hz Limit	Boeing CP

CAM Finite Element Model (NASDA, ARC)

- Detailed model of Centrifuge Accommodation Module including Centrifuge Rotor (Rf. NU-100293, 10/3/2000).
- CAM module generated based on the test-verified JEM-PM model.
- Includes detailed Centrifuge rack model and concentrated mass representation of other rack models.
- Craig-Bampton modal reduction performed on integrated CAM,

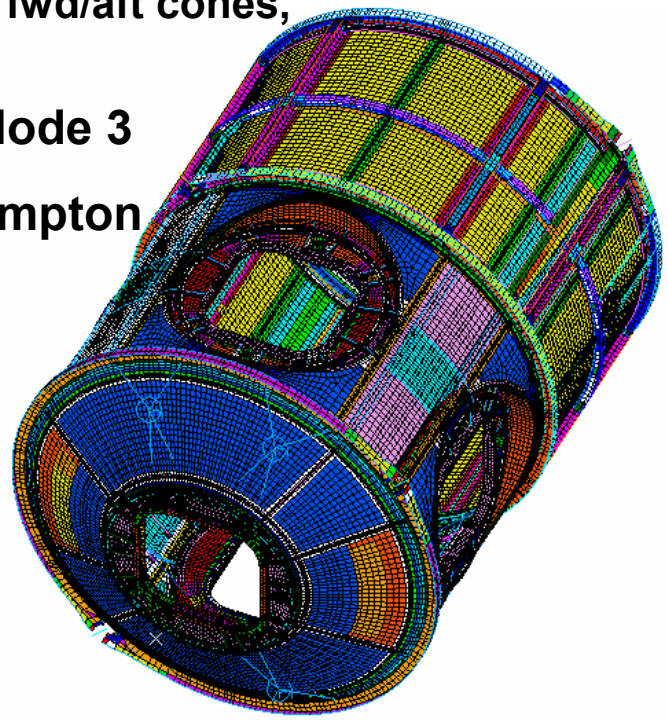
  modal content: 665 modes to 100 Hz .





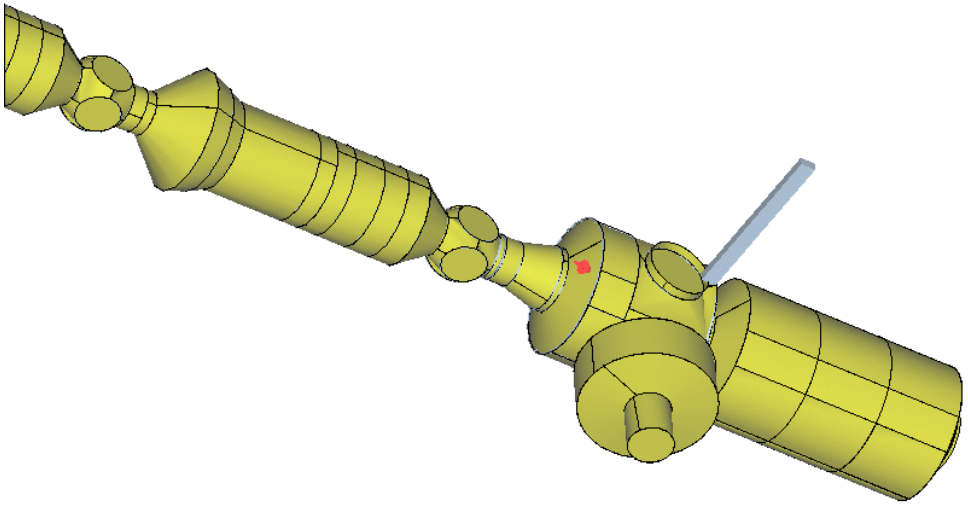
Node 2 Finite Element Model (Alenia, MSFC)

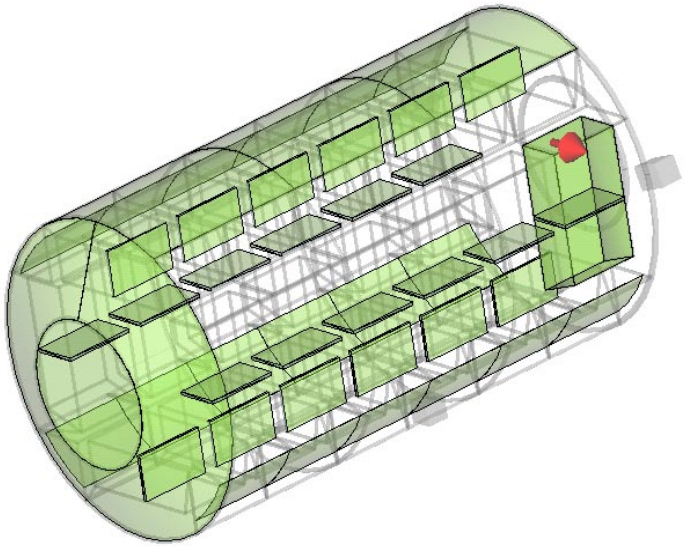
- Detailed model of Node 2 developed by Alenia (Rf. N2-RP-AI-0070, 2/1/2001, N2-RP-AI-0115, 2/23/2001).
- Model includes all primary and secondary structures
  - standoffs, mid-bay & alcove structure, fwd/aft cones, 4 DDCU racks, ISPR
- Identical model used for Node 2 and Node 3
- Model provided by Alenia as Craig-Bampton reduced mass and stiffness matrices.
  - modal content: 301 modes to 57 Hz



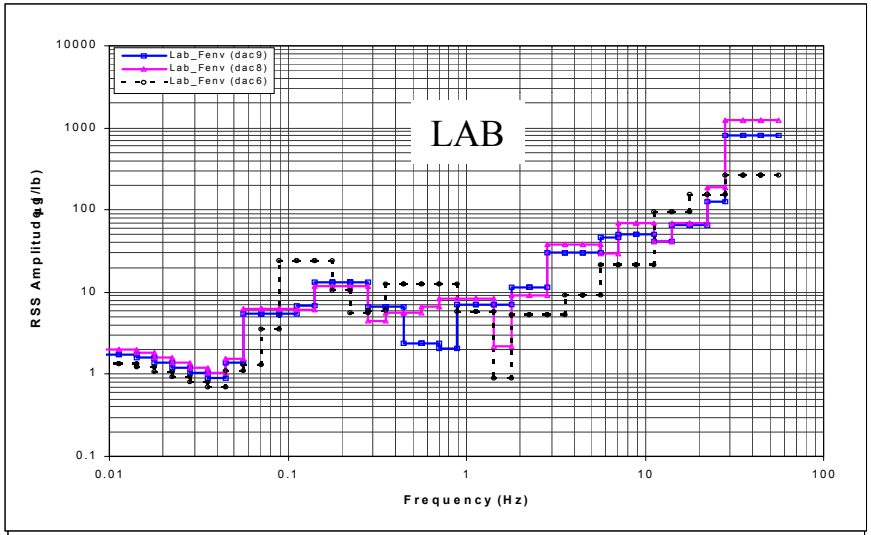
DAC9 Statistical Energy Model Still In Development

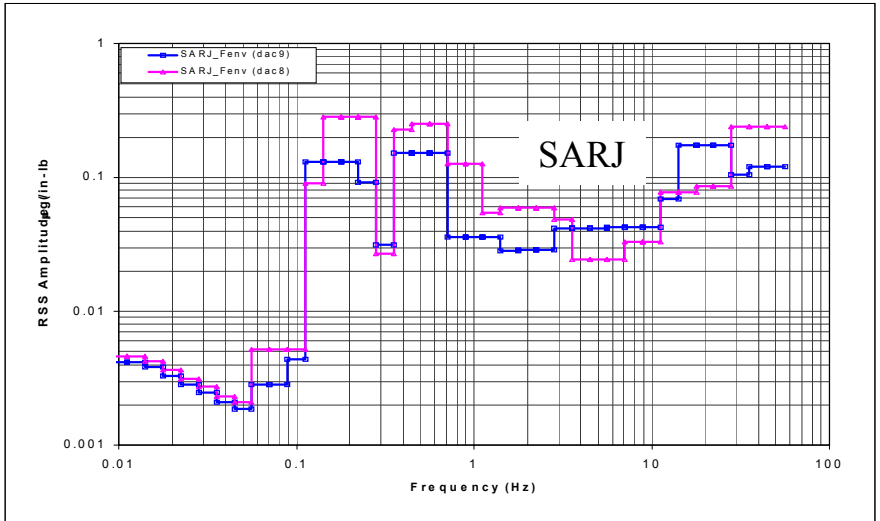
- AutoSEAII software version developed from “drawings”. Software lacked upward compatibility.
- Some variability from ground correlated AutoSEAI model.
- Performing AutoSEAII correlation and update with on-orbit data prior to implementation.

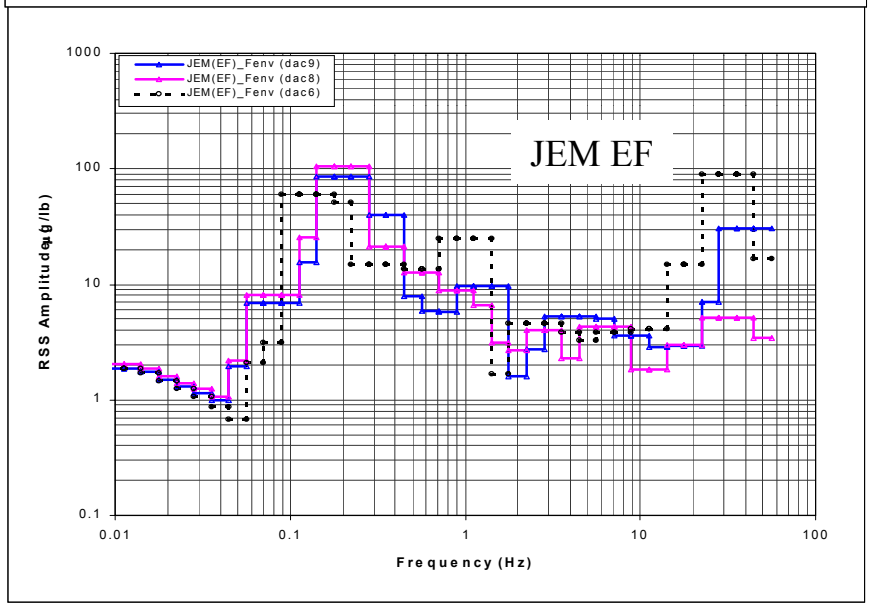


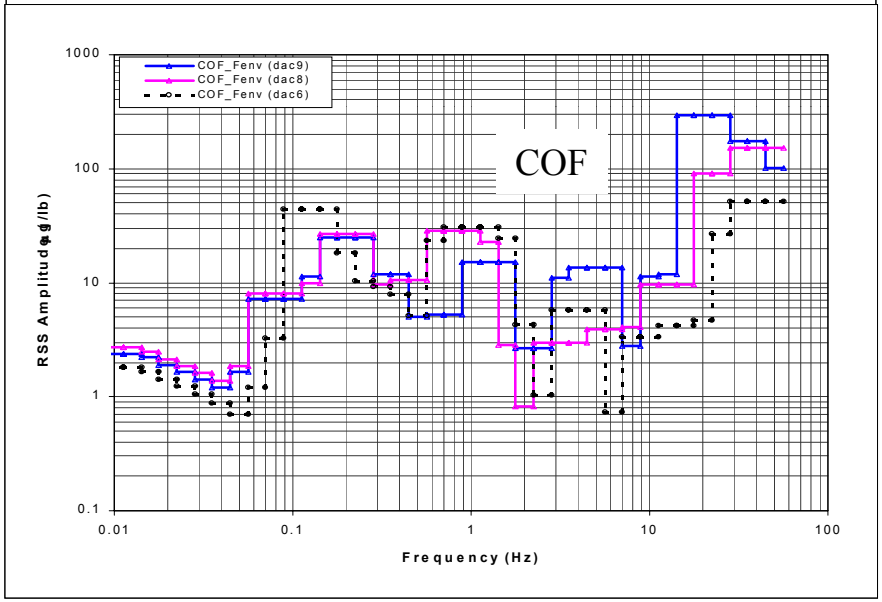


DAC9 FEM Transfer Functions



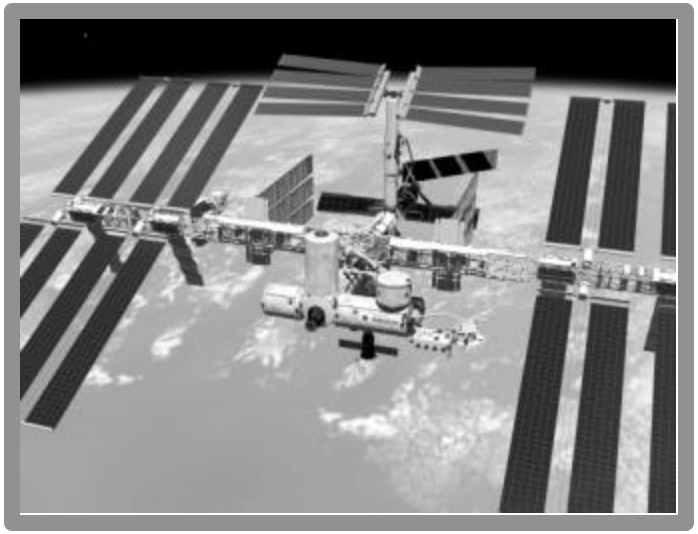






Requirements Apply to the Assembly Complete Configuration

- **1,000,000 lb versus current 300,000 lb**



AC 2007

7A July 2001

Space Station Multi-Rigid Body Simulation (SSMRBS) Parameters

- Component mass properties and projected flat plate areas
- Atmospheric density and momentum exchange characteristic (diffuse/specular)
- Torque equilibrium attitude controller

Measurement Sources

- Operational Data Request Center (ODRC)
  - Appendage position and rate
  - Vehicle position and velocity @ 1 Hz
    (Measured daily from Russian ground track and then numerically propagated)
  - Vehicle attitude and attitude rate errors @ 1 Hz
    (Measured twice daily by Russian star sensors and then propagated from integrated gyro rate measurement data)

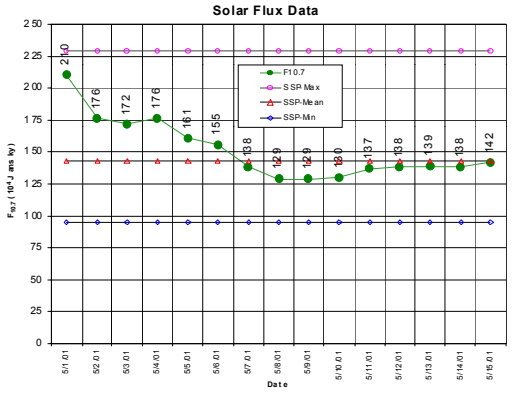
QUASI-STEADY
Simulation & Measurement

- Principal Investigator Microgravity Services (PIMS)
  - Orbital Acceleration Research Experiment (OARE) Sensor Subsystem (OSS) tri-axial accelerations
  - Located in EXPRESS rack drawer in Lab Overhead 2 position
  - Collected at 10 Hz and low pass filtered at 1 Hz

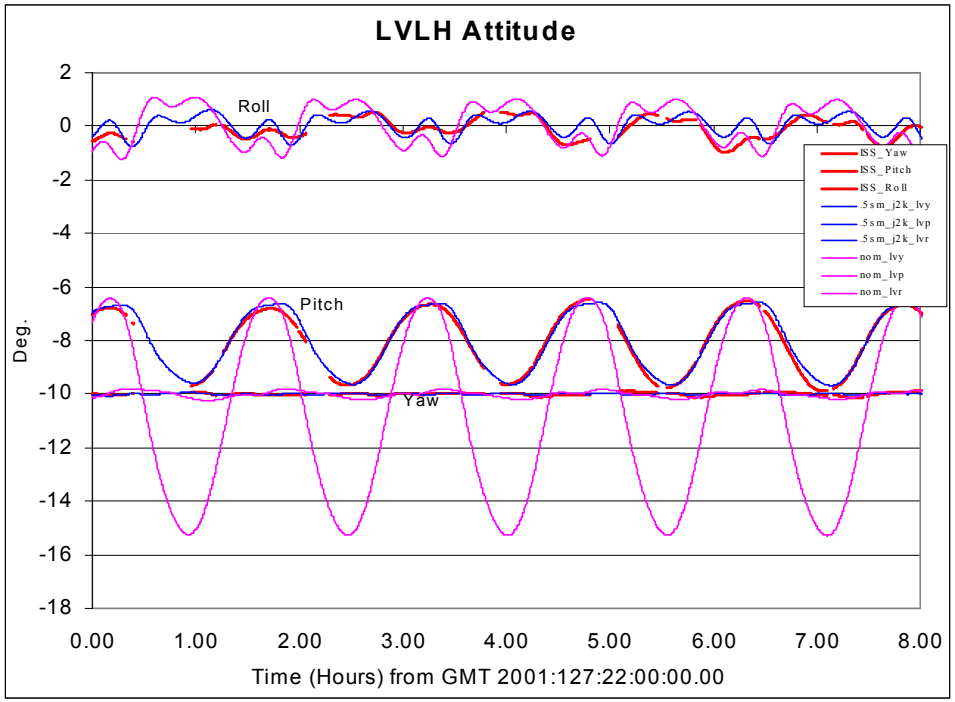
- National Oceanic and Atmospheric Administration (NOAA)
  - Solar flux
  - Geomagnetic index

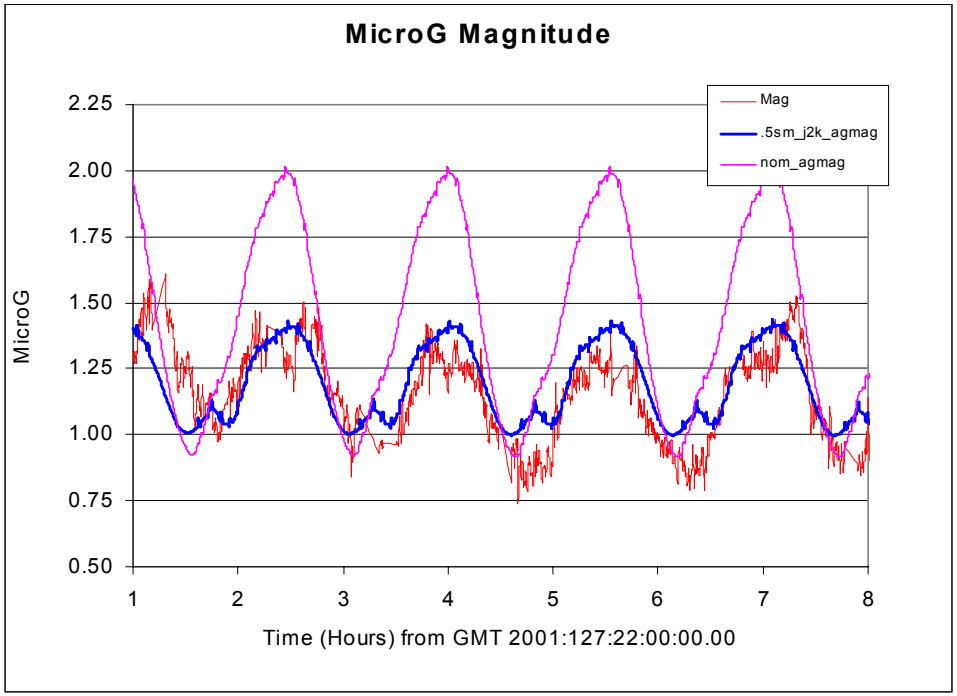
Event #1 - May 7, 2001 - ISS 6A With Crew Asleep - 8 Hours

Inputs	Nom	.5sm_j2k	.5sm_j2k_Δag
Ephemeris Data	Altitude Curve: µg Control Plan 230 nmi 0 Deg. Solar Beta	ODRC: J2K ISS Telemetry 202.78 Nmi 22.5 Deg. Solar Beta	ODRC: J2K ISS Telemetry 202.78 Nmi 22.5 Deg. Solar Beta
Attitude	Simulated	Simulated	Simulated
Solar Flux	Maximum: $F_{10.7}$ 229.1 / A_p 21.2	Actual: $F_{10.7}$ 138 / A_p 11	Actual: $F_{10.7}$ 138 / A_p 11
Solar array	4B and 2B both rotating	4B locked at 47.5 degrees 2B rotating	4B locked at 47.5 degre 2B rotating
Mass Property	DAC8 Databook: ISS_x = -36.8 ISS_y = -0.10 ISS_z = 8.52 Mass = 250,651.5 lbs.	ODRC: ISS_x = -38.58 ISS_y = -0.07 ISS_z = 8.33 Mass = 250,651.5 lbs.	ODRC: ISS_x = -38.58 ISS_y = -0.07 ISS_z = 8.33 Mass = 250,651.5 lbs.
MAMS Location	ISS_x = 11.27 ISS_y = -0.89 ISS_z = 11.01	ISS_x = 11.27 ISS_y = -0.89 ISS_z = 11.01	ISS_x = 11.27 ISS_y = -2.89 ISS_z = 10.01



QUASI-STEADY Correlation





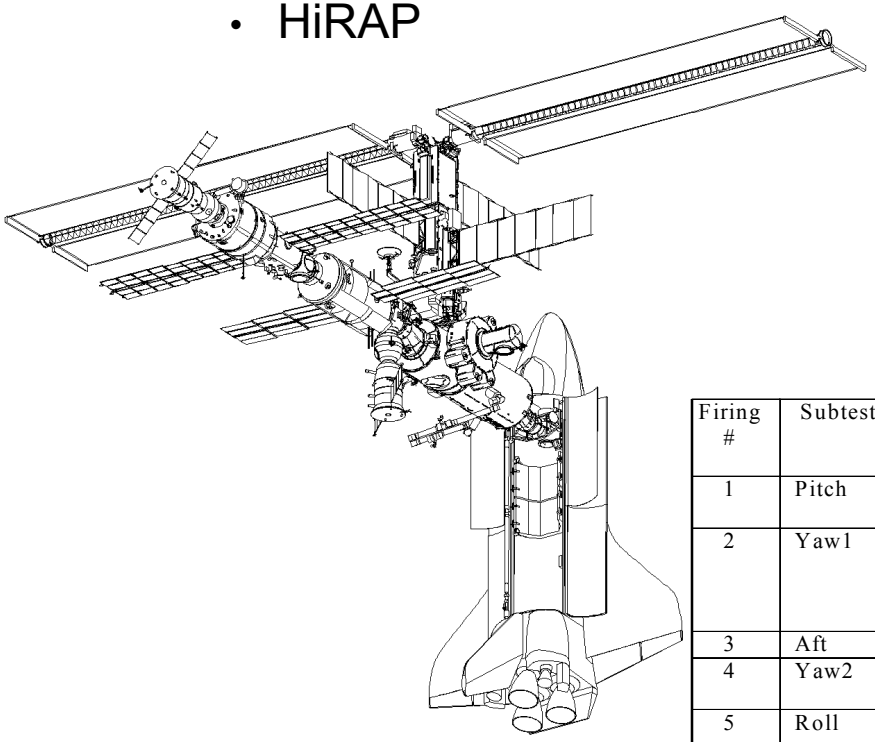
Measurement Sources

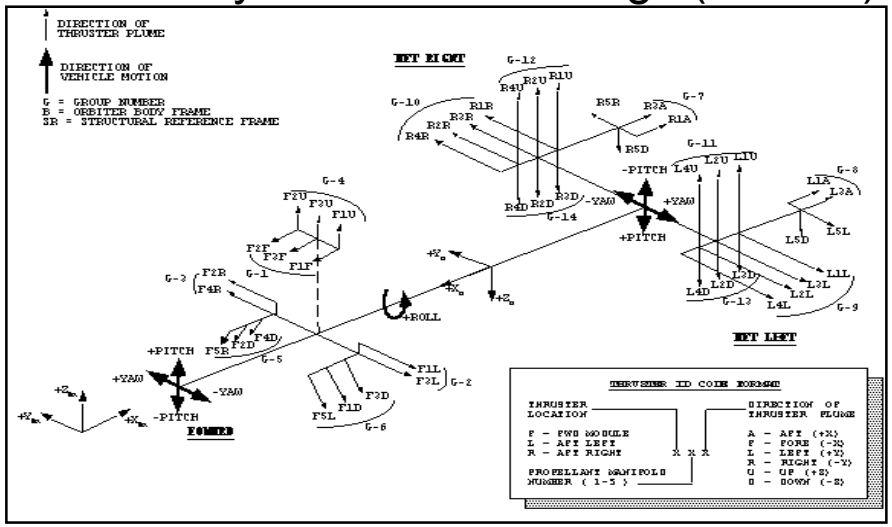
- Operational Data Request Center (ODRC)
  - Appendage position
- Principal Investigator Microgravity Services (PIMS)
  - HiRAP tri-axial accelerometer in EXPRESS rack drawer at Lab Overhead 2 location
  - Space Acceleration Measurement System (SAMS)
    - **3 tri-axial accelerometers on secondary structure interface to racks at Lab Overhead 1&2 locations**
    - **1 tri-axial accelerometer in EXPRESS rack drawer at Lab Overhead 1&2 locations**
- Internal Wireless Instrumentation System (IWIS)
  - 2 tri-axial accelerometers directed at primary structure at fore and aft Node1 locations
  - 2 tri-axial accelerometers directed at primary structure at fore and aft Lab locations
- 60 Potential Russian Data Channels

STRUCTURAL DYNAMIC Correlation

Event #1 - July 17, 2001 - 7A - Station Detailed Test Objective 261

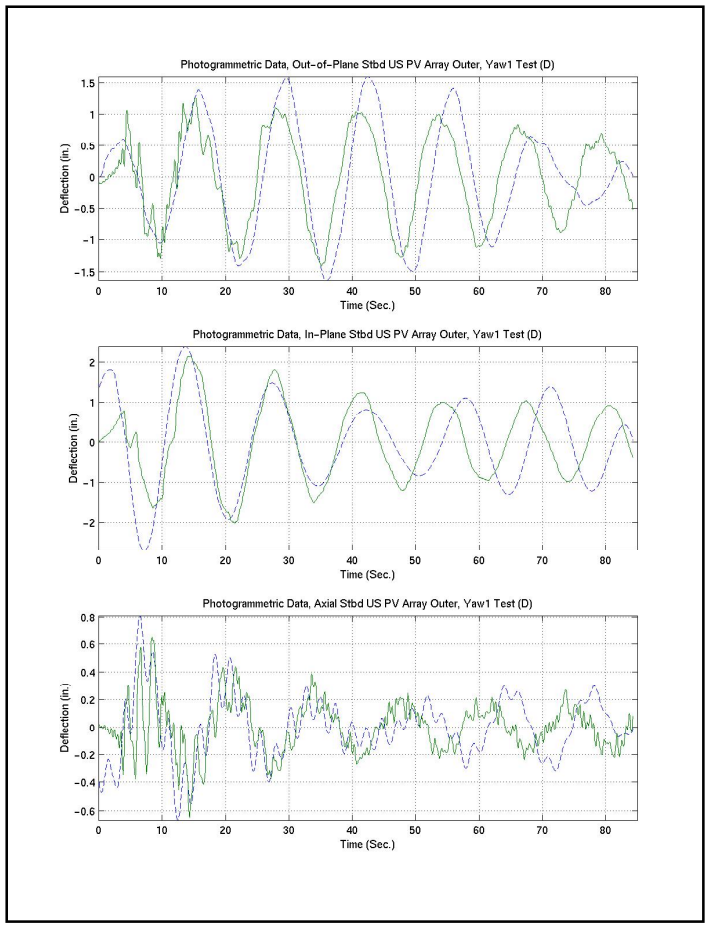
- Shuttle Orbiter Primary Reaction Control System thruster firings (870 lbs)
- Measurements
  - IWIS
  - HiRAP

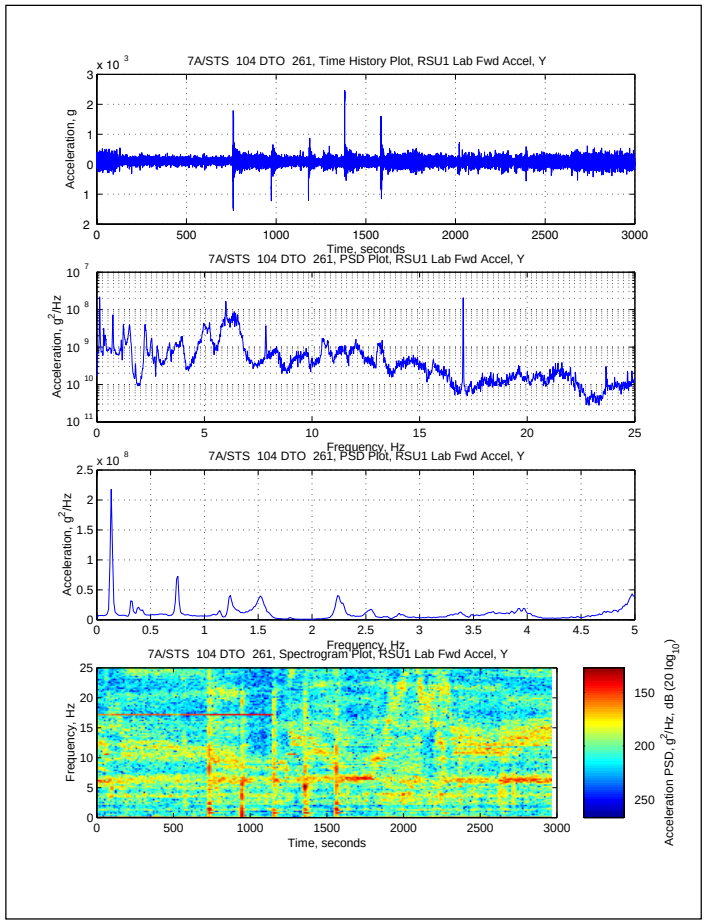




Firing #	Subtest	Jet IDs	Start Time (s)	Pulse Duration (s)	GMT Firing Start Time Day Time Test Day:Hr:Min:Sec	GMT Firing Start Time Night Time Test Day:Hr:Min:Sec
1	Pitch	L1U, R1U	0.00	0.16	343:16:11:25.60	343:18:26:12.55
		L2D, R2D	5.84	0.32	343:16:11:31.44	343:18:26:18.39
2	Yaw1	L1L	0.00	0.24	343:16:18:58.00	343:18:33:42.47
		L1L	1.92	0.24	343:16:18:59.90	343:18:33:44.39
		R1R	6.40	0.24	343:16:19:04.04	343:18:33:48.66
		R1R	8.32	0.24	343:16:19:06.00	343:18:33:50.60
3	Aft	R1A, L1A	0.00	0.24	343:16:26:28.40	343:18:42:03.43
4	Yaw2	L1L	0.00	0.32	343:16:33:58.16	343:18:49:33.35
		R1R	100.0	0.32	343:16:35:40.16	343:18:51:12.95
5	Roll	L2U, R2D	0.00	0.16	343:16:41:28.16	343:18:57:03.11
		L2U, R2D	1.20	0.16	343:16:41:29.36	343:18:57:04.31
		R2D, L2D	6.40	0.16	343:16:41:34.38	343:18:57:09.34
		R2D, L2D	7.60	0.16	343:16:41:35.58	343:18:57:10.54

STRUCTURAL DYNAMIC
Correlation

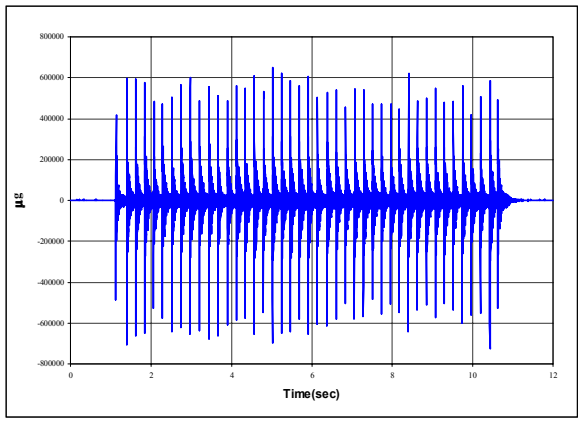


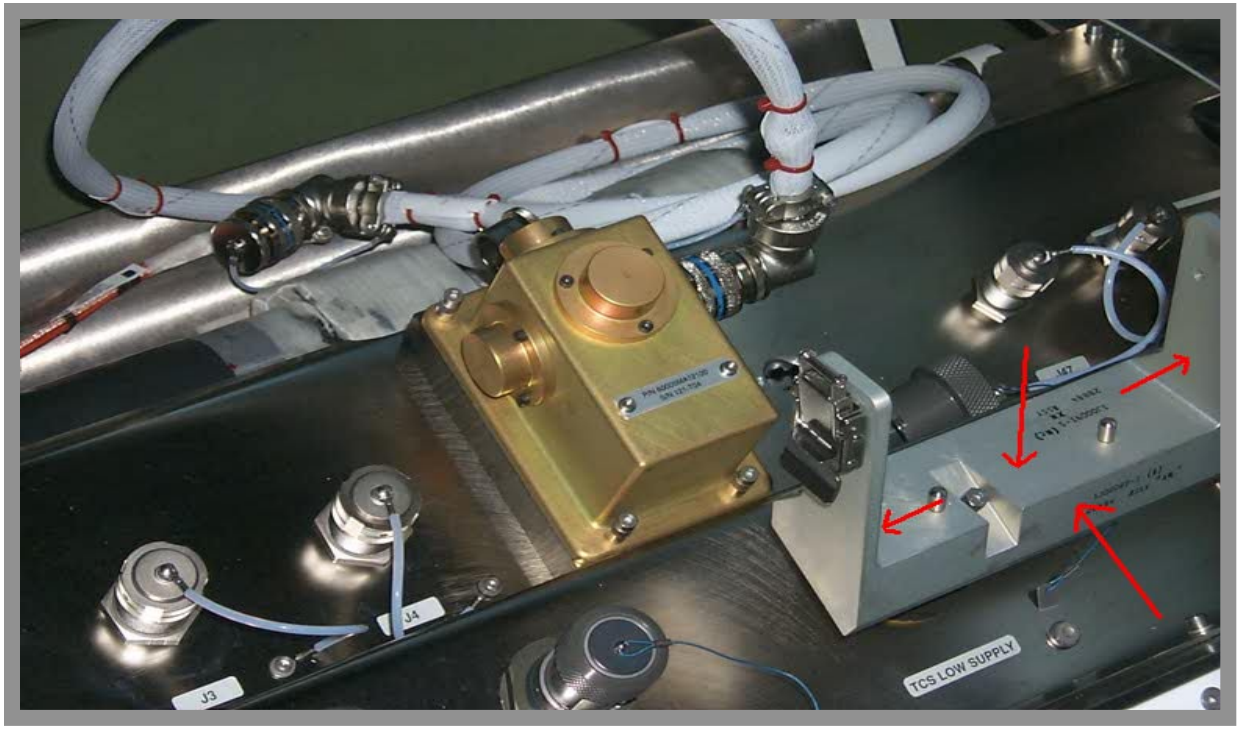


STRUCTURAL DYNAMIC Correlation

Event #2 - October 2, 2001 - 4R - ARIS ICE Hammer Tap

- Crew member hammer tap (uncalibrated) on “Z” Panel at Lab Overhead 1
- Measurements
  - SAMS
  - ARIS





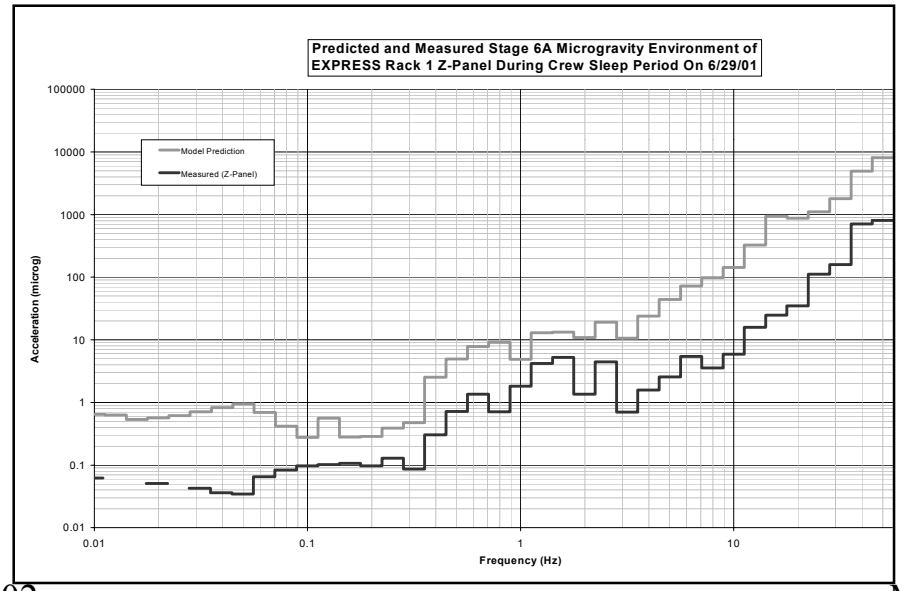
STRUCTURAL DYNAMIC Correlation

Event #3 - TBD 2001 - ARIS ICE Shaker

- Piezoelectric shaker (ground calibrated) on “Z” Panel at Lab Overhead 1
- Measurements
  - SAMS
  - ARIS

Event #4 - June 29, 2001 - 6A - Crew Sleep

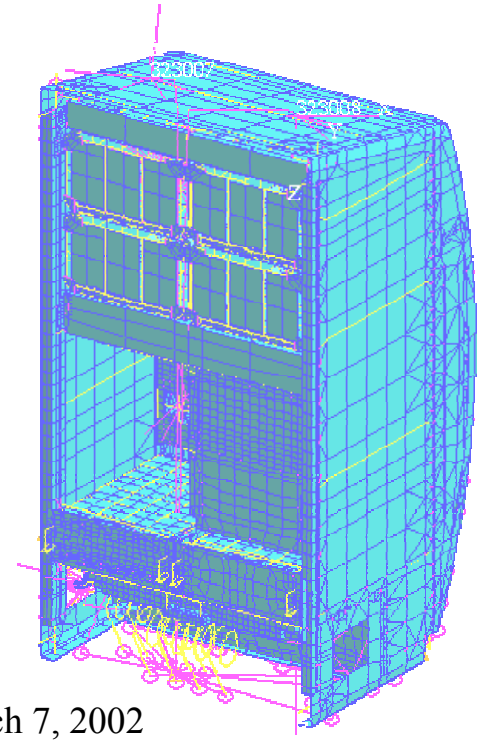
- Ambient acceleration
- Measurement - SAMS “Z” Panel Lab Overhead 1
- Finite element predictions based on 1999 (DAC8) results

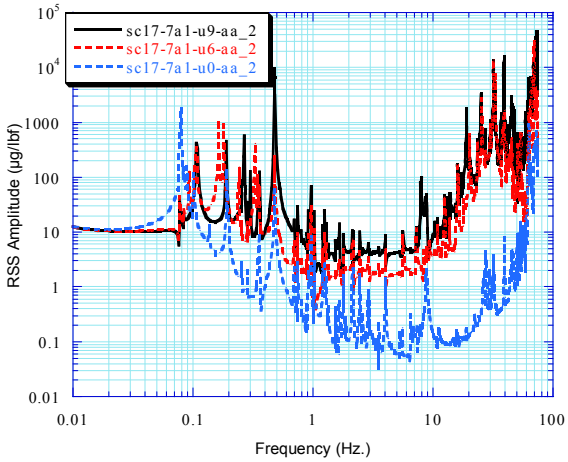


STRUCTURAL DYNAMIC Update

Boeing Loads and Dynamics Team responsible for model correlation and update for primary load bearing modes, typically below 10 Hz

Boeing Microgravity Team working secondary structure correlation and update, typically above 1 Hz



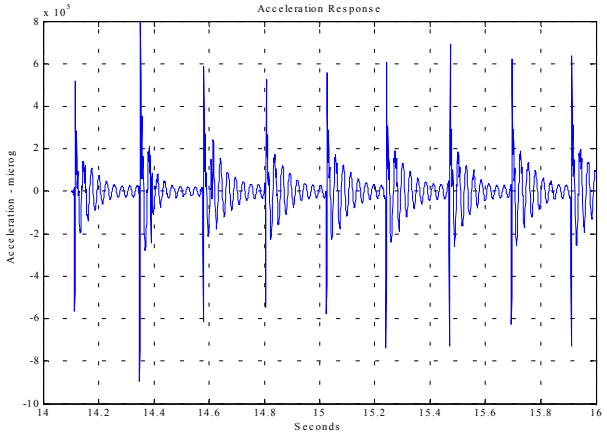


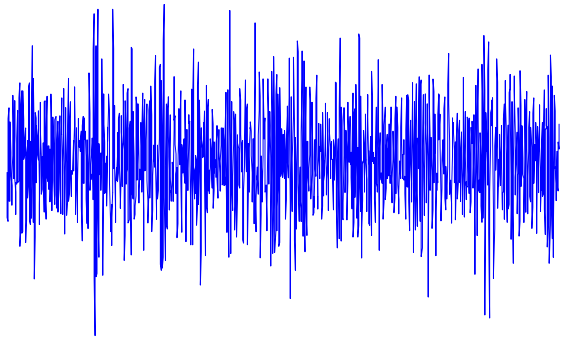
9 - 6 - 0 Baseline Umbilical Cases For "Y" Shaker @ "Z" Panel Input

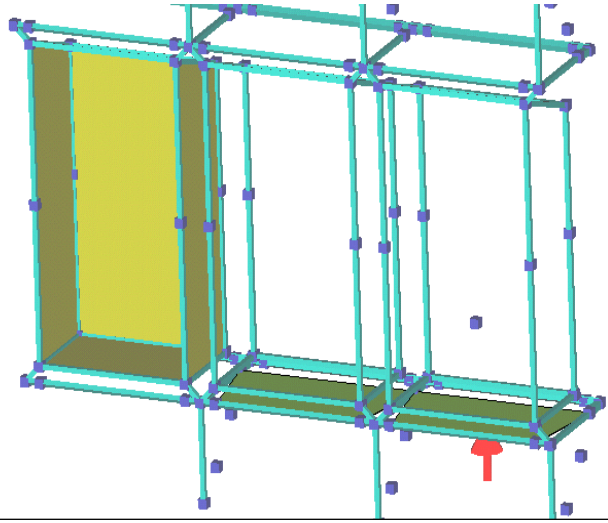
VIBROACOUSTIC
Correlation & Update

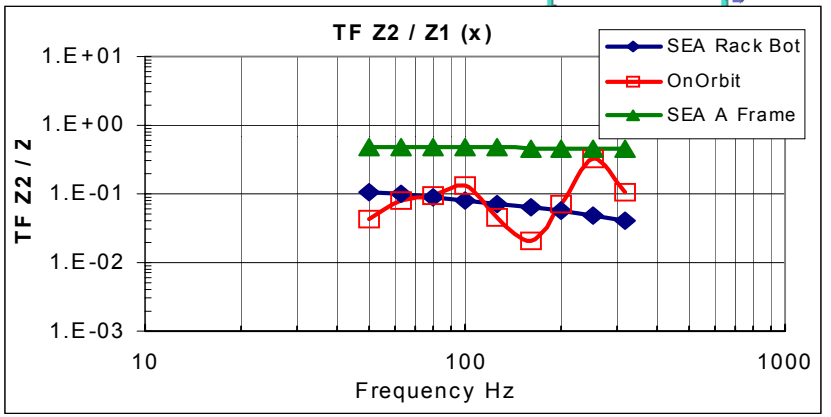
Event #1 - October 2, 2001 - 4R - ARIS ICE Hammer Tap

- Crew member hammer tap (uncalibrated) on “Z” Panel at Lab Overhead 1
- Measurements SAMS and ARIS

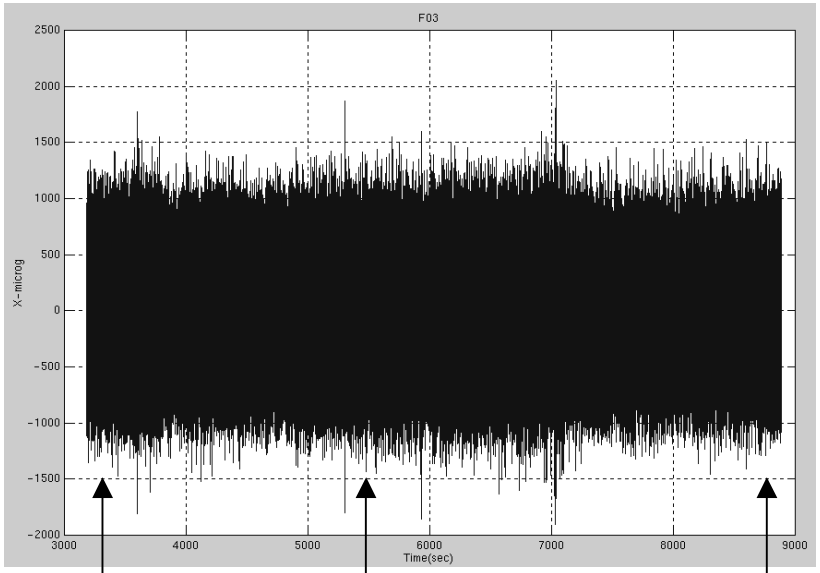


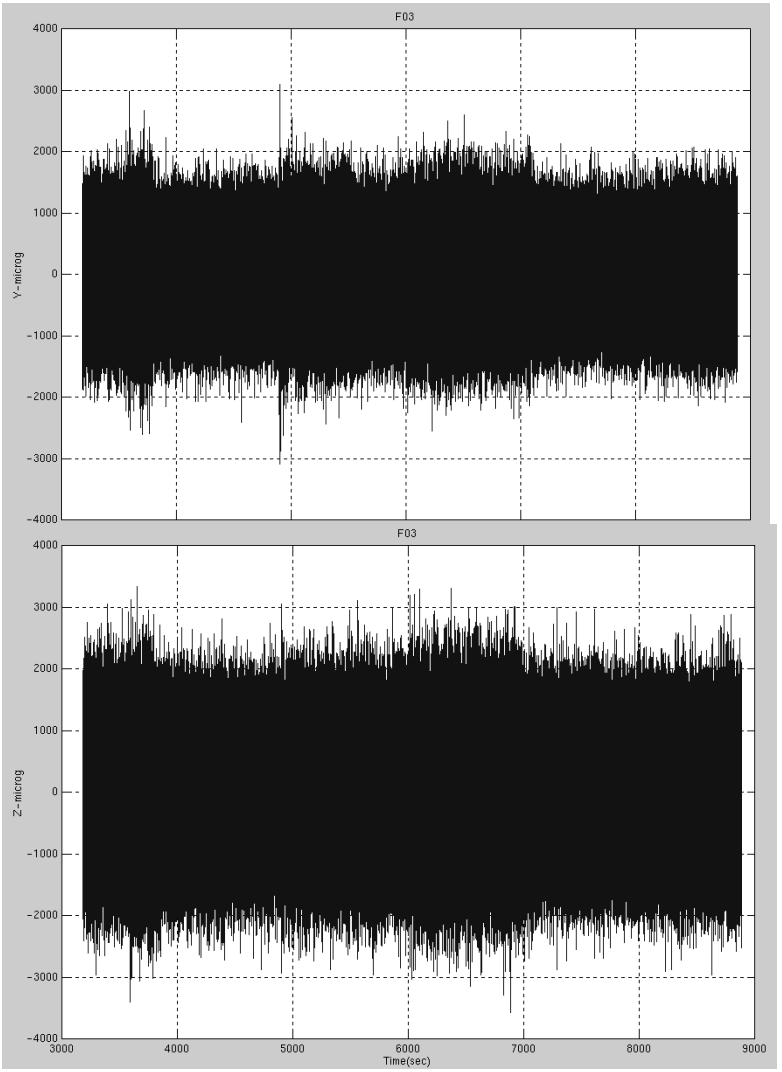






UF1 Vibratory Measured Data
Exhibits No Significant Day/Night Variation



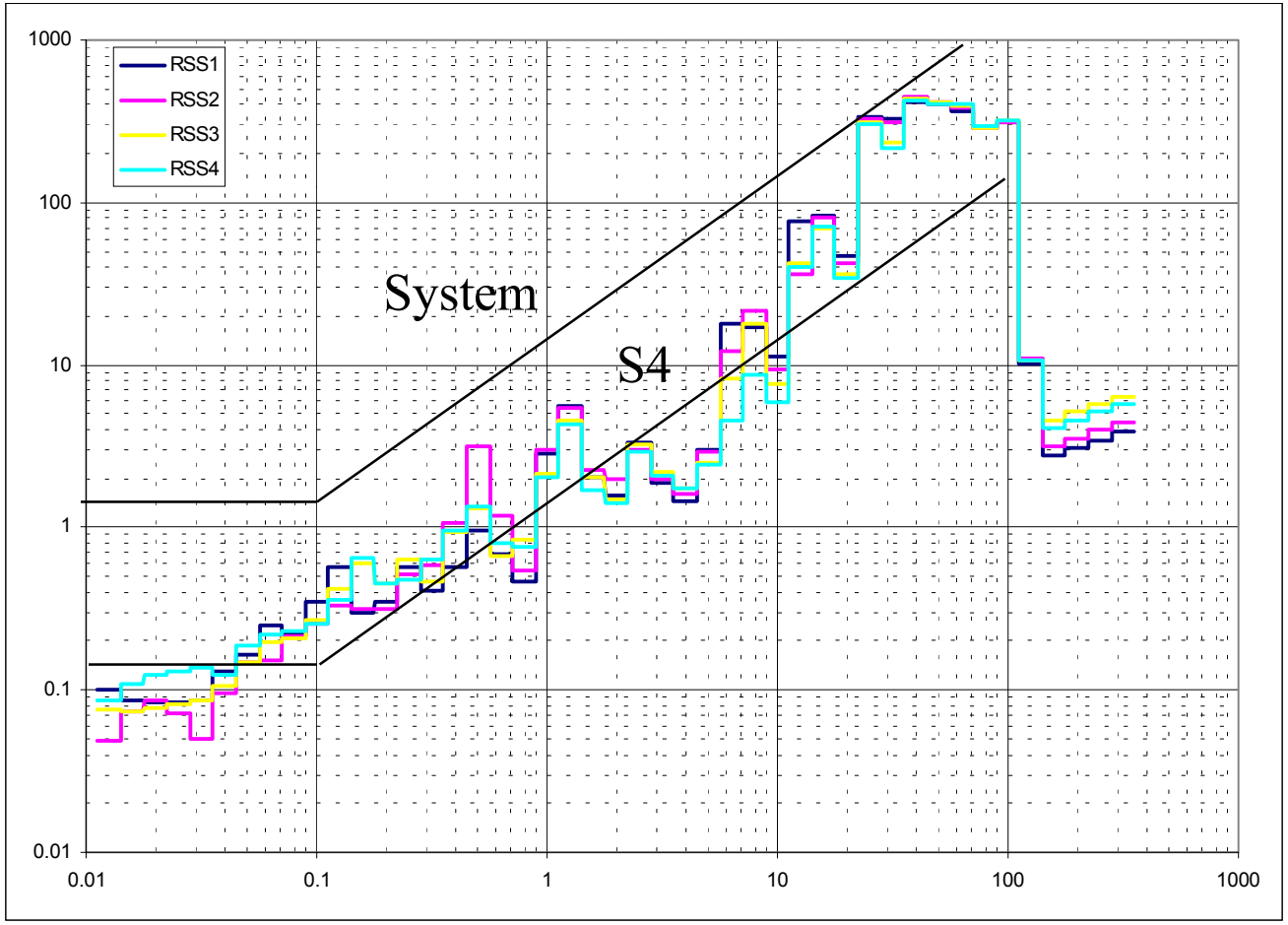


UF1 SAMS LO1 Z-Panel

- December 18, 2001 GMT 01:00:00
- Both Arrays Rotating Once/Orbit
- Torque Equilibrium Attitude
- Crew Asleep

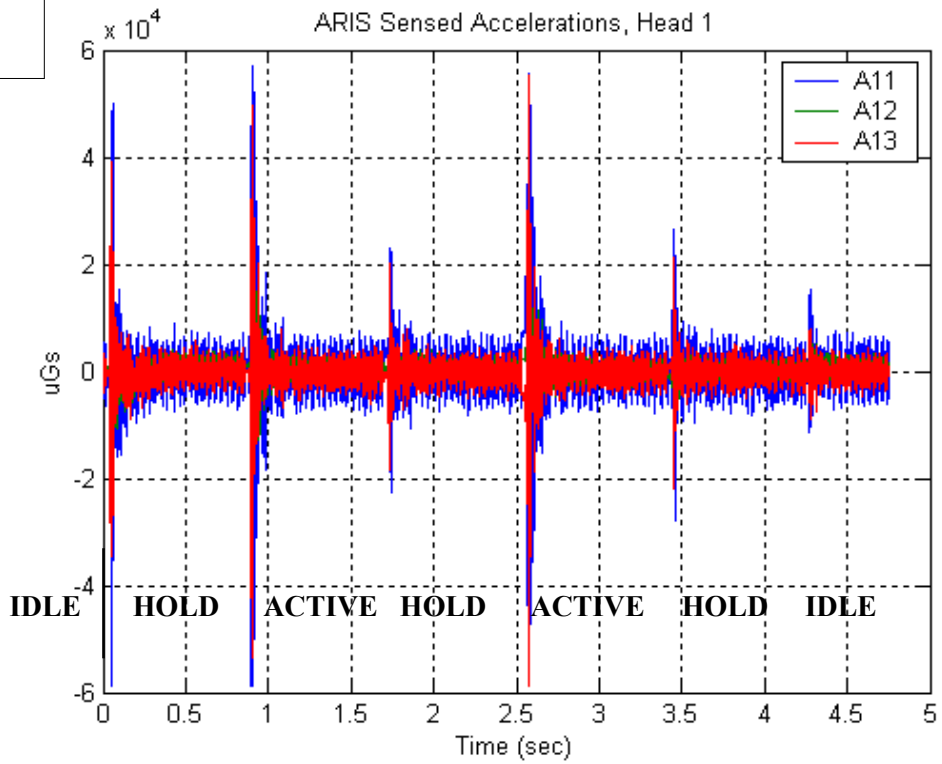
UF1 Vibratory Measured Data Exhibits No Significant Day/Night Variation

- Four - 100 Second Samples About Night/Day 5400 - 5800.
- NO ARIS ISOLATION FACTORS (-20 Db /Decade to -60 Db)
- REQ. SHOWN ONLY FOR ORIENTATION!
- Compliance assessments use 50% of ARIS PIDS isolation.



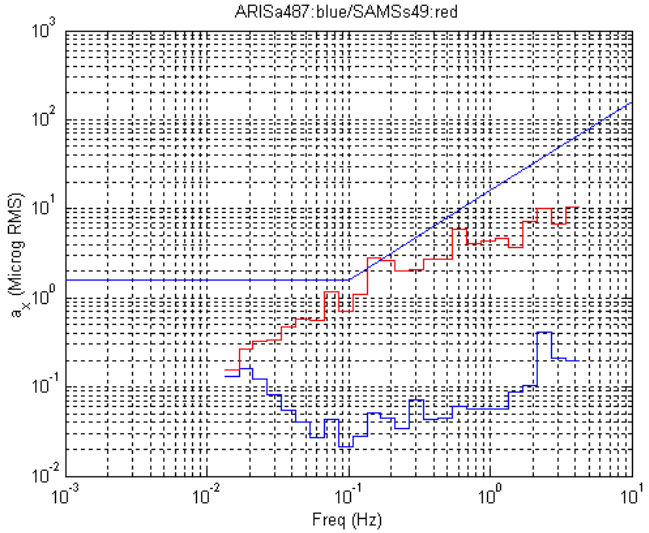
Transition Transient Acceleration

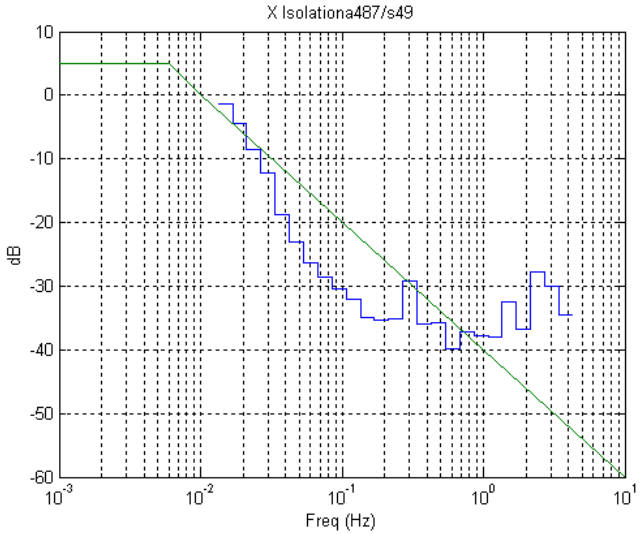
Reference: "ARIS-ICE Flight Operations Overview– August 27, 2001"

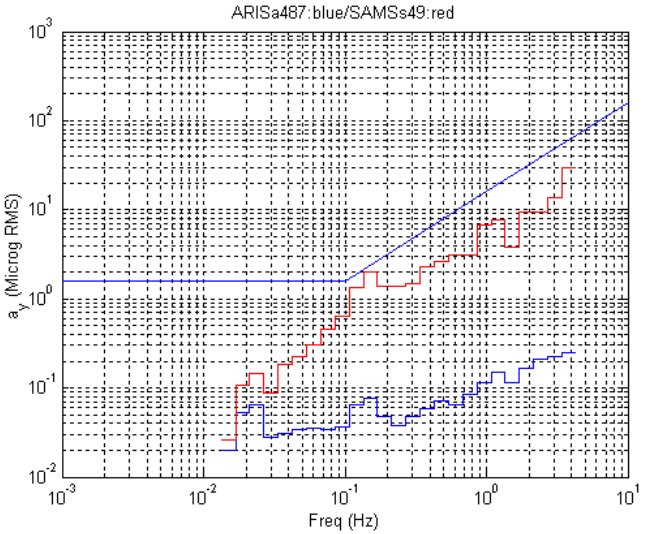


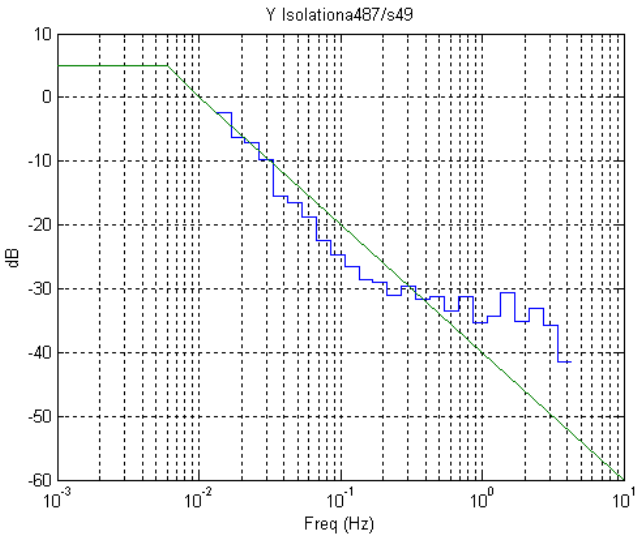
IDLE to HOLD ~ 60 milli-Gs peak
HOLD to ACTIVE ~ 60 milli-Gs peak
ACTIVE to HOLD ~ 30 milli-Gs peak
HOLD to IDLE ~ 10 milli-Gs peak

Isolation Test #a487/s49



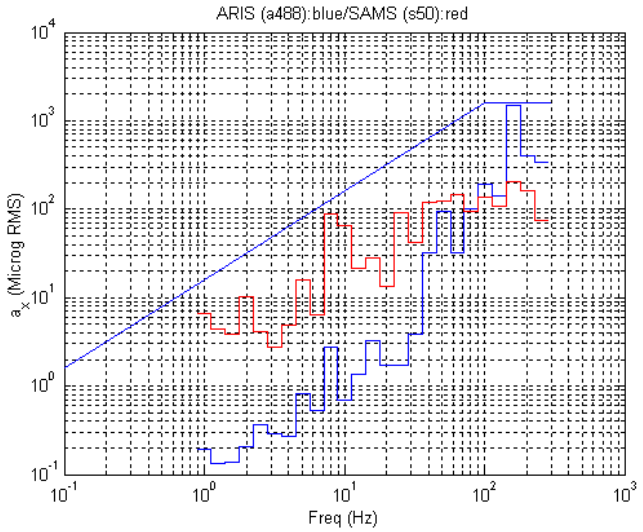


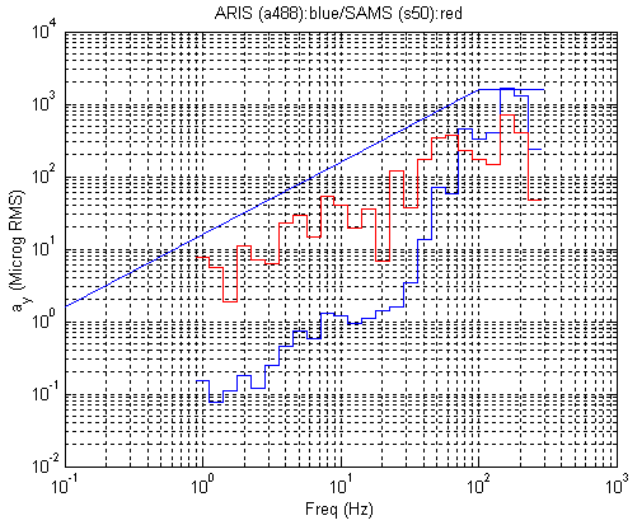


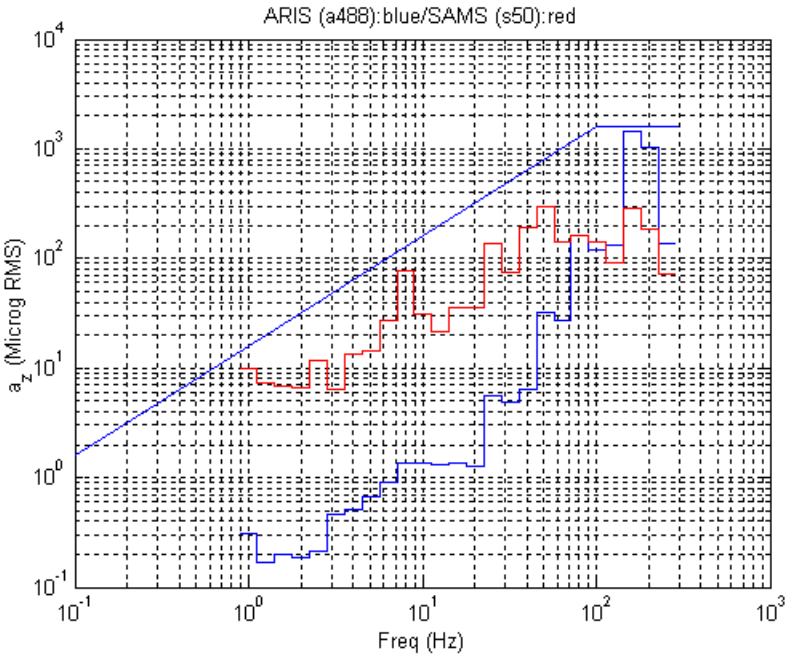


- Frequency range= [.015 - 4] Hz after filter/decimation
- Low frequency isolation consistent with predictions

Isolation Test #a488/s50







- Frequency range after filter/decimation [1-300 Hz]
- Insufficient high frequency energy to resolve isolation.
- On-board acceleration levels generally at least a factor of 10 below ISS requirement curve.
- ICE-Shaker and hammer tap data (analysis in work) will be used to resolve high frequency isolation

Activities Completed

Reference:"ARIS-ICE Status– January 18, 2002"

ARIS-ICE was launched on flight 6A in April 2001

ARIS and ARIS-ICE have to date:

- spent over 10 successful months on orbit in the ISS
- we have logged over 2,300 hours on our ground station console
- transmitting over 15,000 commands (from ground console to ISS)
-conducted over 1,446 ARIS-ICE on orbit tests (and counting)

Including:
- 334 SAMS tests
- 78 ARIS buffer tests (in standard configuration)

Activities Completed

ARIS-ICE activities and testing completed to date:

- Reduced Sway Space Configuration Testing
- ARIS Initial Checkout Tests
- 7-Actuator Testing
- Upper Right Actuator/Pushrod Replacement
- All Hammer Tests for First Umbilical Configuration
- 7A Docked Ops Testing Complete (7 Actuators)
- 7A.1 Docked Ops Testing Complete (8 Actuators)
- All Station Shake Testing
- Improved ARIS' perf - power umbilical design, dev, test and selection
  - ICE's position was to identify and try to improve ARIS' (umbilical) isolation performance in addition to just testing the ARIS baseline
- Upper Left Actuator/Pushrod Replacement.

Upcoming Activities

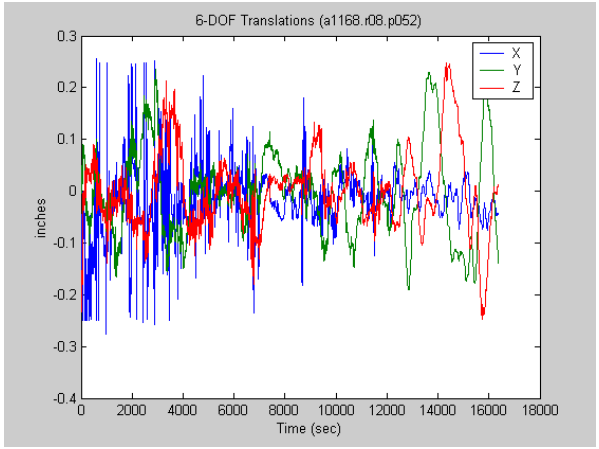
- 01/21/02: Hammer Tests
- TBD (01/21/02 - 01/31/02): ARIS GN2 Umbilical Installed.
- TBD (01/22/02 - 01/31/02): Hammer Tests with GN2 Umbilical.
- 02/01/02 - 02/08/02: ARIS Standard Configuration Testing (RIC Controls ARIS)
- 02/11/02: Return to POP Configuration (ARIS-ICE POP Controls ARIS).
- 02/21/02: Snubber Cup Isolators (Foam Inserts) Installed.
- 02/25/02: Rack Shake Testing Begins.
- 02/26/02: Snubber Cup Isolators Removed.
- 03/05/02: Rack Shake Testing Ends. Shaker Subsystem Stowed.
- 03/06/02: Crew Push-off Tests.
- 8A - UF-2: Support ZCG Microgravity Operations

Accomplishments

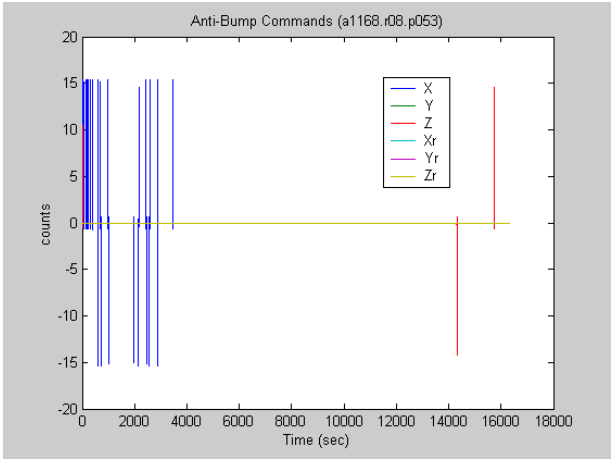
Current status as a result of ARIS-ICE Operations

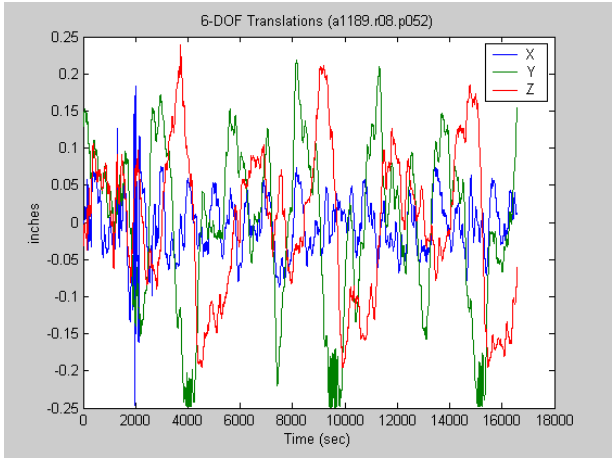
- Have shown redesign of system was successful via on orbit operations
- Have shown the ARIS controller is stable in orbit over a 10 month period
- Have validated performance of ARIS across 0-300 Hz frequency range
  - With exception of 1-10 Hz window which is being worked now
- Have confirmed robustness of ARIS' conventional controller on orbit
- Have developed H infinity controller and run it on orbit successfully
- Have demonstrated the STS79 pushrod actuator problem has been corrected
- ICE demonstrated ARIS is functional-- some issues will still require work
  - i.e. elimination of transition transients, system issues (certain frequency windows) may need to be addressed by MIPT etc.

ICE “Quiescent” Measurements



A1168
10/26 - 21:37:08
XPOP





A1189
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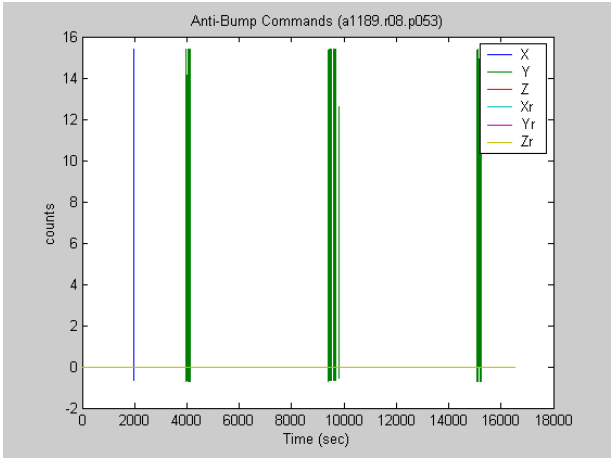
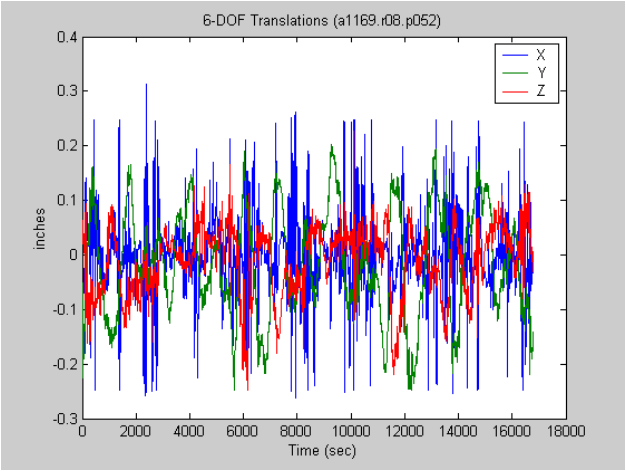


ICE "Awake" Measurements



A1169
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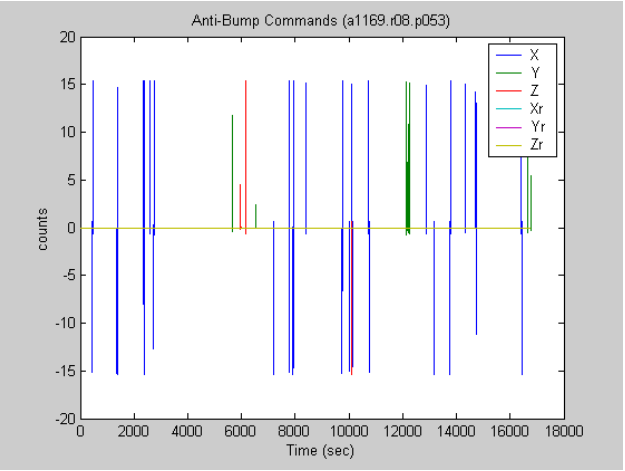
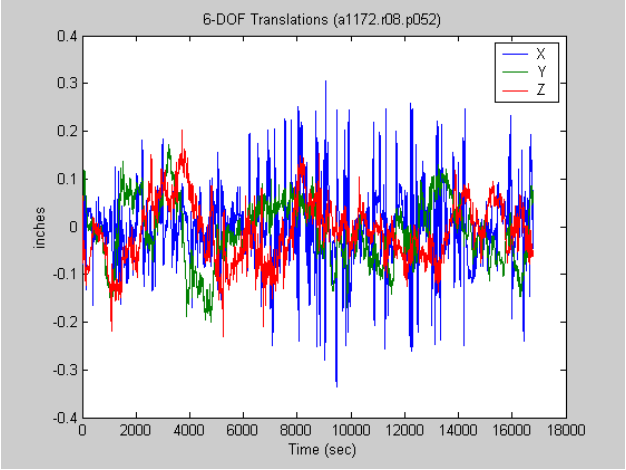
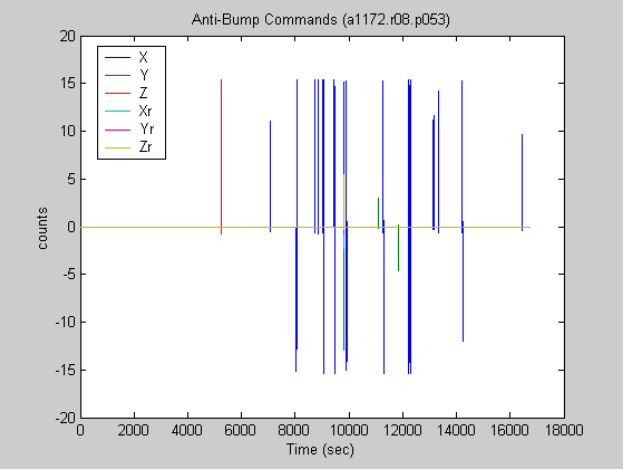




A1172
10/28 - 09:02:19
XPOP



The ISS vehicle has been designed to provide researchers a viable microgravity environment established jointly with the science community.

- **Features:**
  - Laboratories located near the vehicle center of mass
  - Articulating photovoltaic and radiator appendages to enable once per orbit vehicle rotation
  - Non-propulsive attitude control
  - Source isolated exercise equipment
  - Receiver isolation systems
  - Microgravity Mode operations
- **Design Convergence:**
  - Requirements
  - Control Plan
  - Key Ground Tests
    - Control Moment Gyros
    - Rotating Joints
    - Node1
    - Service Module
    - Lab
    - COF sub-systems
  - Verification

Summary (continued)

Payload microgravity requirements have been approved for pressurized payloads and S3 attached payloads.

ARIS ICE preliminary reports are positive with regard to isolation performance capability. Only the 1 to 10 Hz region is yet to be characterized. Long duration operability lessons are still being given.

Assembly stage acceleration data has supported analytical trends and reduced the uncertainty and risk associated with PV Array thermal induced vibrations and RTAS (P6-Z1) stick/slip disturbance sources.

Key threats & planned/recommended countermeasures:

- **Service Module air conditioner compressor non-compliance - Approved ground test and on-orbit installation of vibration mounts and extended fluid flex lines.**
- **Service Module ergometer non-compliance with verified ARIS performance. - Pursue early measurements to confirm predictions and resolve if necessary.**
- **U.S. Lab ergometer non-compliance due to rack to pivot pin impact. - - Pursue early measurements to confirm predictions and resolve if necessary.**
- **Payload disturbances, payload rack structural dynamics. - Work requirement definition and verification process.**

Summary (continued)

Sustaining Engineering Underway:

- **Use early on-orbit measurement data to establish confidence in analytical models**
  - **Complete 7A suite of model correlation and update activity**
  - **Next focus on 13A with symmetric inboard truss assembled**
- **Support operations**
  - **Excessive "x" sway space motion**
- **Perform anomaly resolution**
  - **Evaluate acceptability of less than 1/2 inch sway space**
- **Insure Assembly Complete compliance**
  - **Utilize updated "plant" models**
  - **Re-evaluate forcing functions based on on-orbit performance**
  - **Evaluate U.S. Core Complete Assembly Sequence impacts**

Acronyms

CoFR : Certification of Flight Readiness
COF : Columbus Orbital Facility
GN&C: Guidance, Navigation, and Control
IRD : Interface Requirements Document
JEM : Japanese Experiment Module
PD : Payload Developer
PIA : Payload Integration Agreement
PEI : Payload Engineering Integration
POIC : Payload Operations Integration Center
RS : Russian Segment
SSP : Space Station Program
USOS: United States On-orbit Segment